

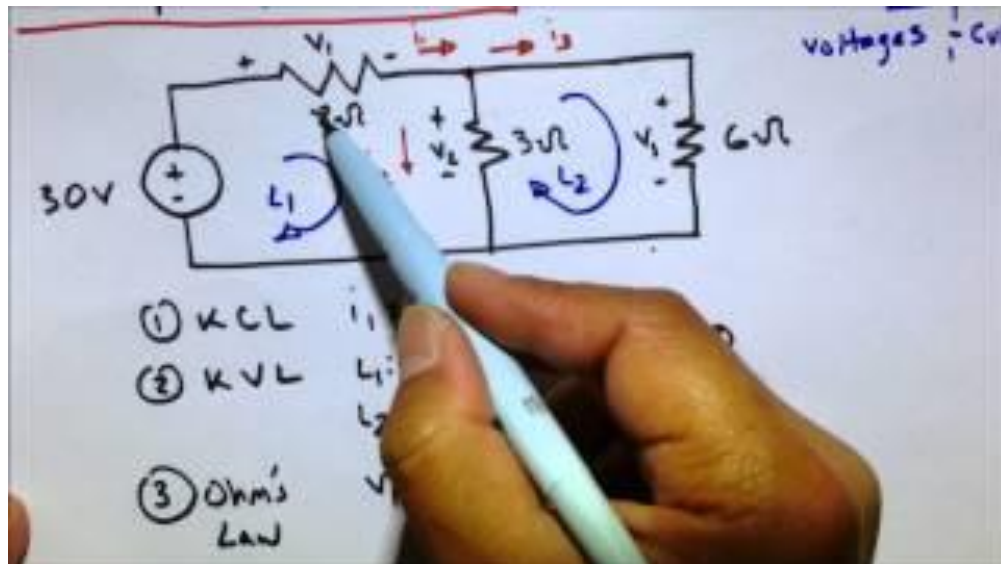


DR. GYURCSEK ISTVÁN

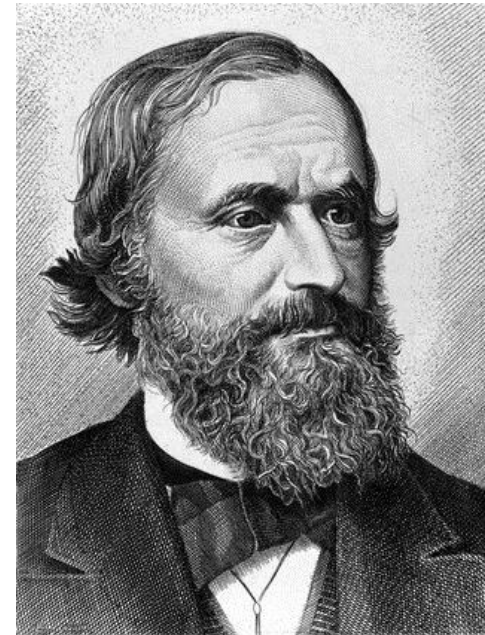
# Methods of Circuit Analysis

## *Sources and additional materials (recommended)*

- ❑ *Dr. Gyurcsek – Dr. Elmer: Theories in Electric Circuits, GlobeEdit, 2016, ISBN:978-3-330-71341-3*
- ❑ *Ch. Alexander, M. Sadiku: Fundamentals of Electric Circuits, 6th Ed., McGraw Hill NY 2016, ISBN: 978-0078028229*
- ❑ *Simonyi K.: Villamosságtan. AK Budapest 1983, ISBN:9630534134*
- ❑ *Dr. Selmeczi K. – Schnöller A.: Villamosságtan 1. MK Budapest 2002, TK szám: 49203/I*
- ❑ *Dr. Selmeczi K. – Schnöller A.: Villamosságtan 2. TK Budapest 2002, ISBN:9631026043*
- ❑ *Zombory L.: Elektromágneses terek. MK Budapest 2006, ([www.electro.uni-miskolc.hu](http://www.electro.uni-miskolc.hu))*



KCL + KVL + Characteristics → WORKS ... (but difficult)



„Alternatives’ ...

## METHODS

- Nodal analysis
- Mesh analysis

## THEOREMS

- *Superposition theorem*
- *Thevenin's theorem*
- *Norton's theorem*
- *Source transform*

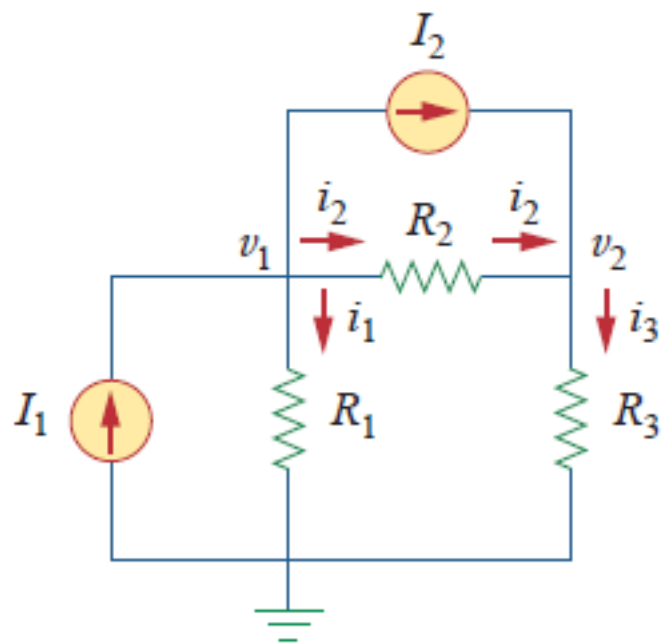
# KCL + KVL + CHAR



- Nodal Analysis**
- Mesh Analysis
- Applications (*DC Transistor Circuits*)

# Nodal Analysis

- ❑ Goal → determining each **nodal voltage** (one is reference = 0 V)
- ❑ Symbols for reference node (GND)



**node 1** →  $I_1 = I_2 + i_1 + i_2$

**node 2** →  $I_2 + i_2 = i_3$



*principle* →  $i = \frac{v_{higher} - v_{lower}}{R}$

**node 1** →  $I_1 = I_2 + \frac{v_1}{R_1} + \frac{v_1 - v_2}{R_2}$

→  $I_1 = I_2 + v_1 G_1 + G_2(v_1 - v_2)$

**node 2** →  $I_2 + \frac{v_1 - v_2}{R_2} = \frac{v_2}{R_3}$

→  $I_2 + G_2(v_1 - v_2) = G_3 v_2$

$$(G_1 + G_2)v_1 - G_2 v_2 = I_1 - I_2$$

$$-G_2 v_1 + (G_2 + G_3)v_2 = I_2$$

$$\begin{bmatrix} G_1 + G_2 & -G_2 \\ -G_2 & G_2 + G_3 \end{bmatrix} \cdot \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} I_1 - I_2 \\ I_2 \end{bmatrix}$$

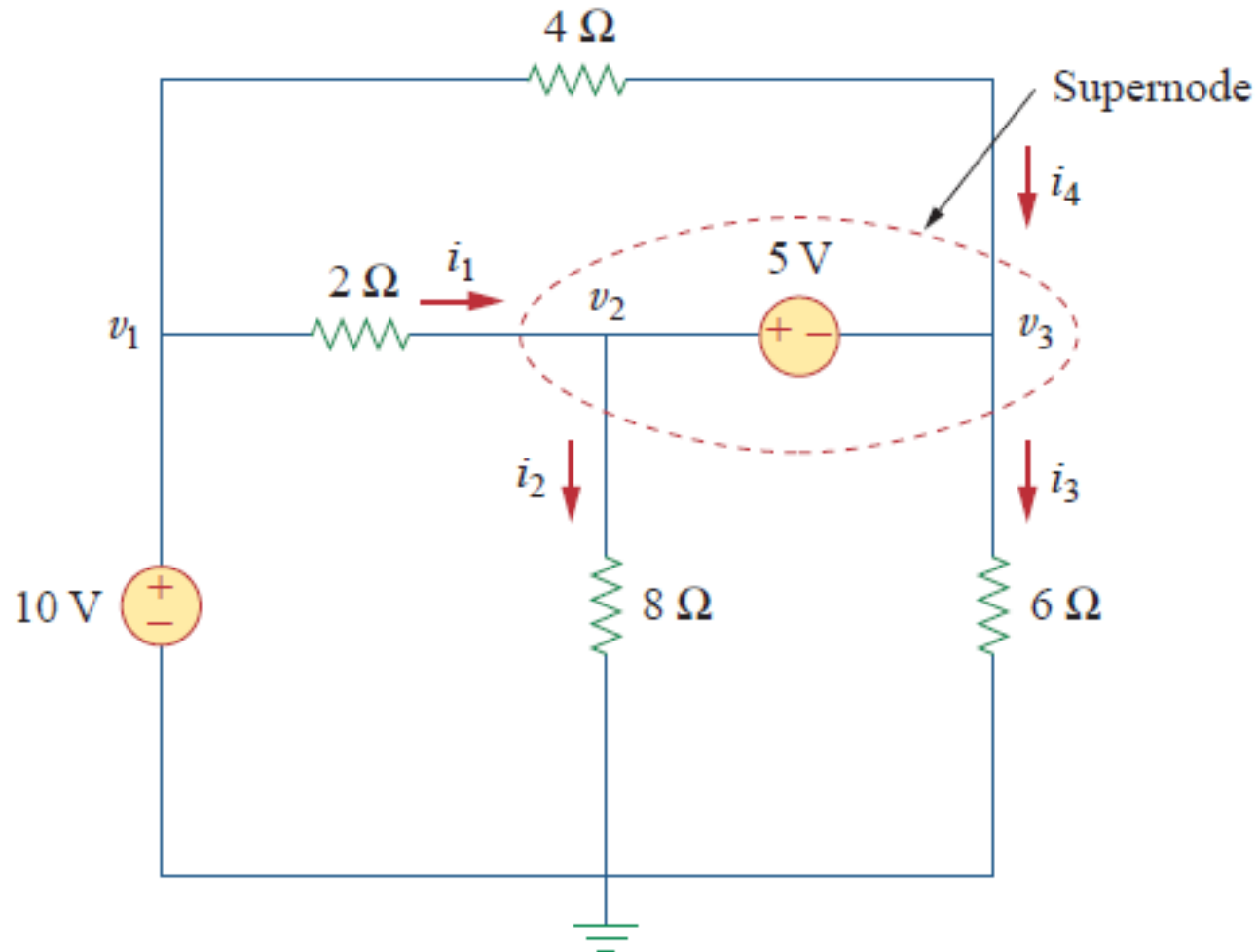
*Cramer's rule* →  $v_1 = \frac{\Delta_1}{\Delta}$ ,  $v_2 = \frac{\Delta_2}{\Delta}$

$$\Delta = \det \begin{bmatrix} G_1 + G_2 & -G_2 \\ -G_2 & G_2 + G_3 \end{bmatrix}$$

$$\Delta_1 = \det \begin{bmatrix} I_1 - I_2 & -G_2 \\ I_2 & G_2 + G_3 \end{bmatrix}$$

$$\Delta_2 = \det \begin{bmatrix} G_1 + G_2 & I_1 - I_2 \\ -G_2 & I_2 \end{bmatrix}$$

## Nodal Analysis with Voltage Sources – Supernode



❑ CASE 1 → Voltage source bw. node and ref. node

$$(eq. 1): v_1 = 10 V$$

❑ CASE 2 → Voltage source bw. two nodes

$v_2; v_3 \rightarrow$  form super node

$$i_1 + i_4 = i_2 + i_3 \rightarrow$$

$$(eq. 2): \frac{v_1 - v_2}{2} + \frac{v_1 - v_3}{4} = \frac{v_2 - 0}{8} + \frac{v_3 - 0}{6}$$

$$(eq. 3): v_2 - v_3 = 5 \text{ (additional KVL!)}$$

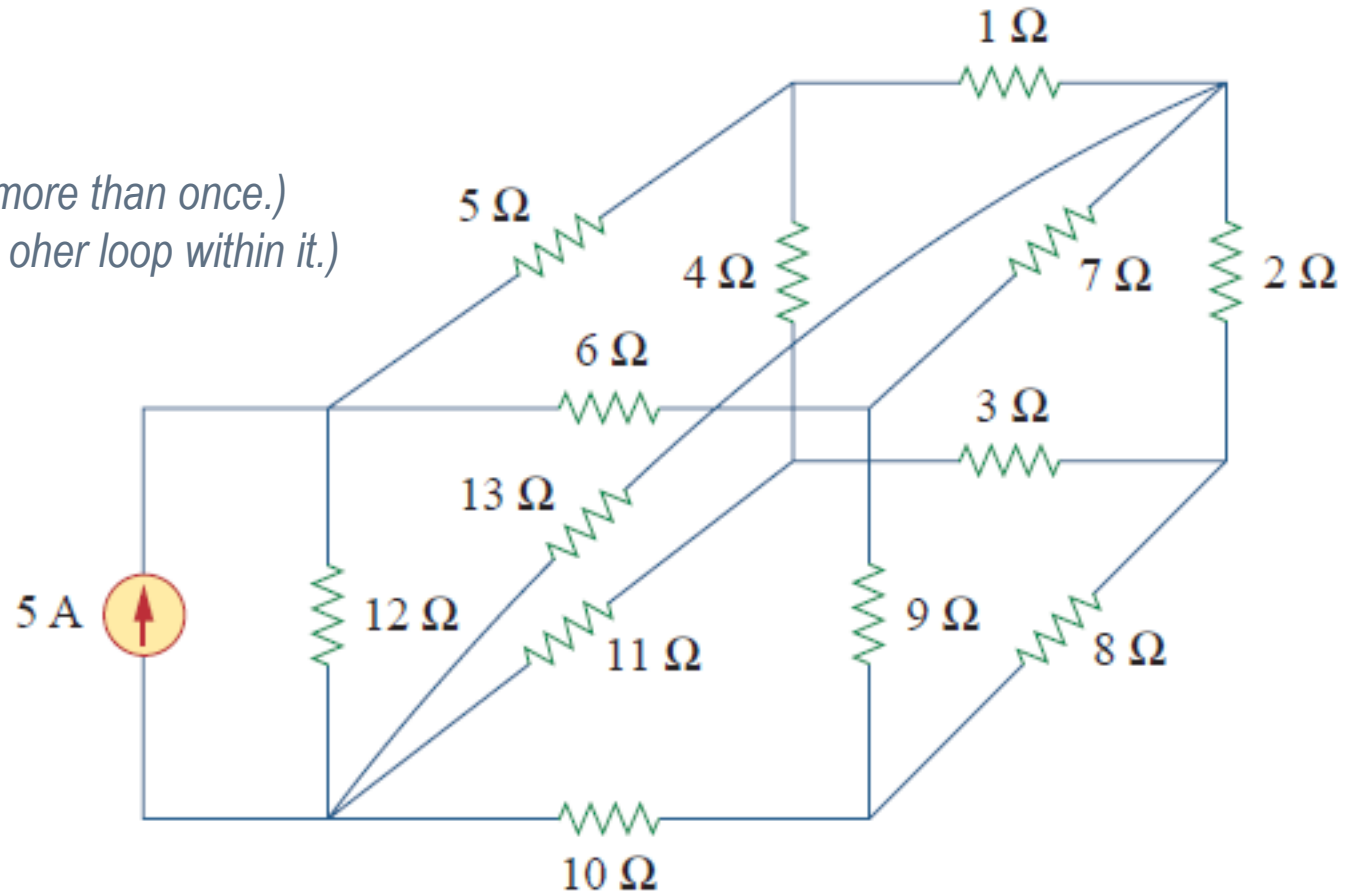


- Nodal Analysis
- Mesh Analysis**
- Applications (*DC Transistor Circuits*)

# Mesh Analysis

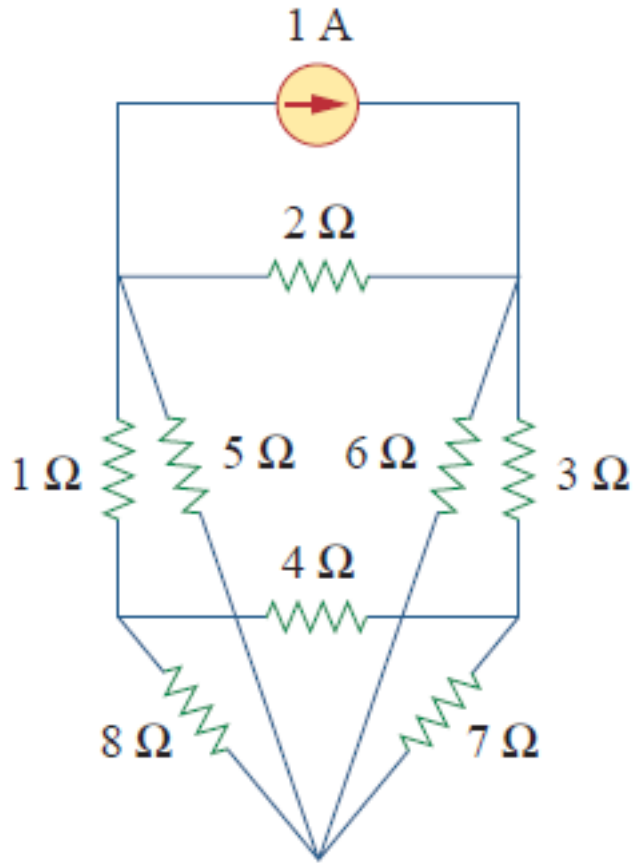
- ❑ Mesh current  $\rightarrow$  circuit variable
- ❑ (*Loop  $\rightarrow$  closed path, no node passed more than once.*)
- ❑ (*Mesh  $\rightarrow$  loop that does not contain any other loop within it.*)

Mesh analysis  $\rightarrow$   
easy to use for planar circuits!  
*(nonplanar: can't be drawn in plain w/o crossing branches)*



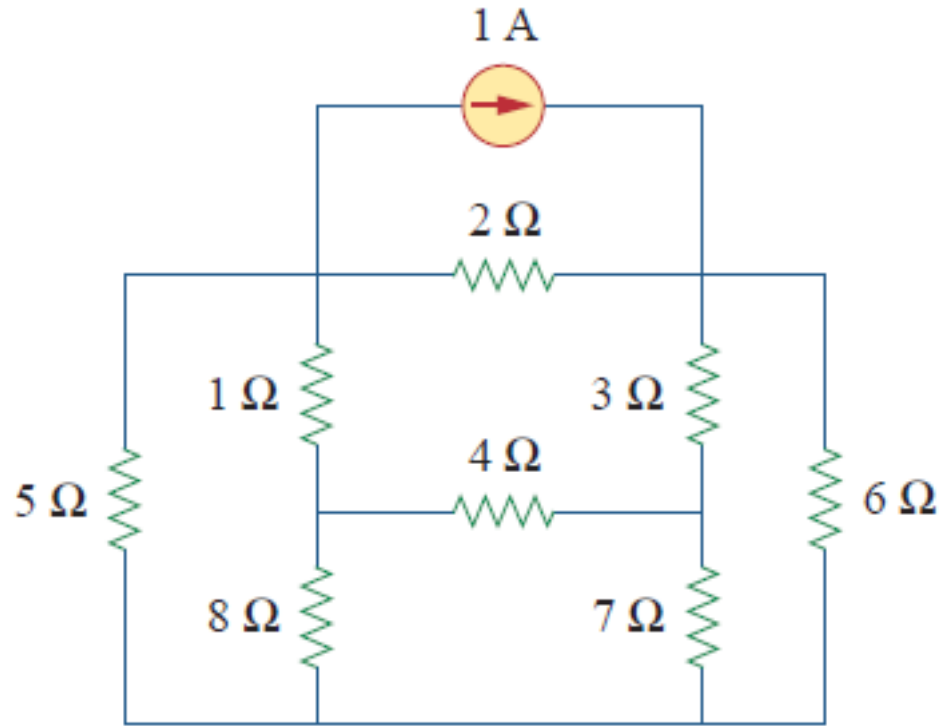
# Example for Planar Circuit

Seems to be nonplanar



→ REDRAW →

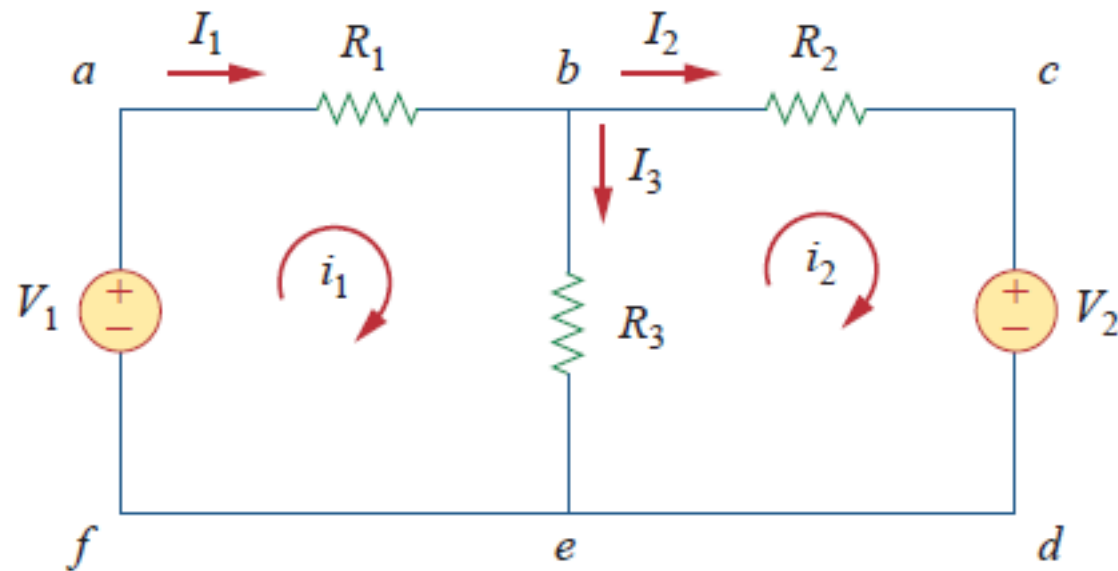
planar





# Mesh Analysis

Mesh  $\rightarrow$  'window'



$$-V_1 + R_1 i_1 + R_3(i_1 - i_2) = 0 \rightarrow (R_1 + R_3)i_1 - R_3 i_2 = V_1$$

$$R_2 i_2 + V_2 + R_3(i_2 - i_1) = 0 \rightarrow -R_3 i_1 + (R_2 + R_3)i_2 = -V_2$$

$$\begin{bmatrix} R_1 + R_3 & -R_3 \\ -R_3 & R_2 + R_3 \end{bmatrix} \cdot \begin{bmatrix} i_1 \\ i_2 \end{bmatrix} = \begin{bmatrix} V_1 \\ -V_2 \end{bmatrix}$$

Cramer's rule  $\rightarrow i_1 = \frac{\Delta_1}{\Delta}, i_2 = \frac{\Delta_2}{\Delta}$

$$\Delta = \det \begin{bmatrix} R_1 + R_3 & -R_2 \\ -R_2 & R_2 + R_3 \end{bmatrix}$$

$$\Delta_1 = \det \begin{bmatrix} V_1 & -R_2 \\ -V_2 & R_2 + R_3 \end{bmatrix}$$

$$\Delta_2 = \det \begin{bmatrix} R_1 + R_3 & V_1 \\ -R_2 & -V_2 \end{bmatrix}$$

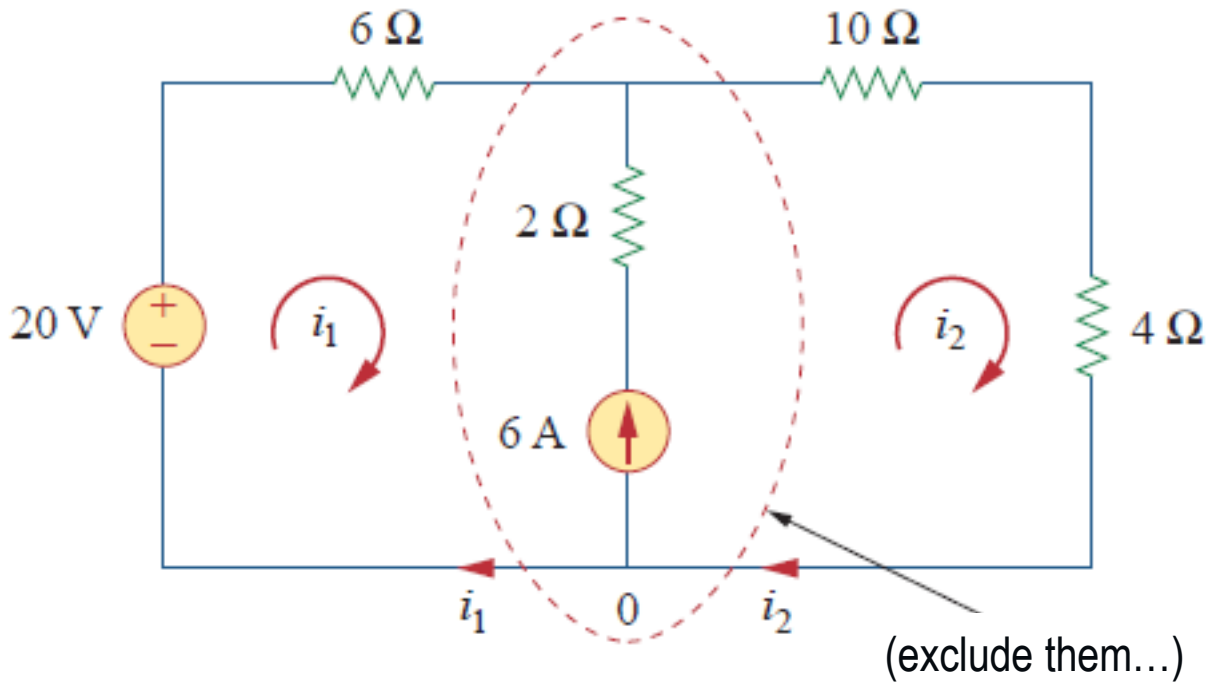
**Last step!**  $\rightarrow I_1 = i_1, I_2 = i_2, I_3 = i_1 - i_2$

## Mesh Analysis with Current Sources – Supermesh

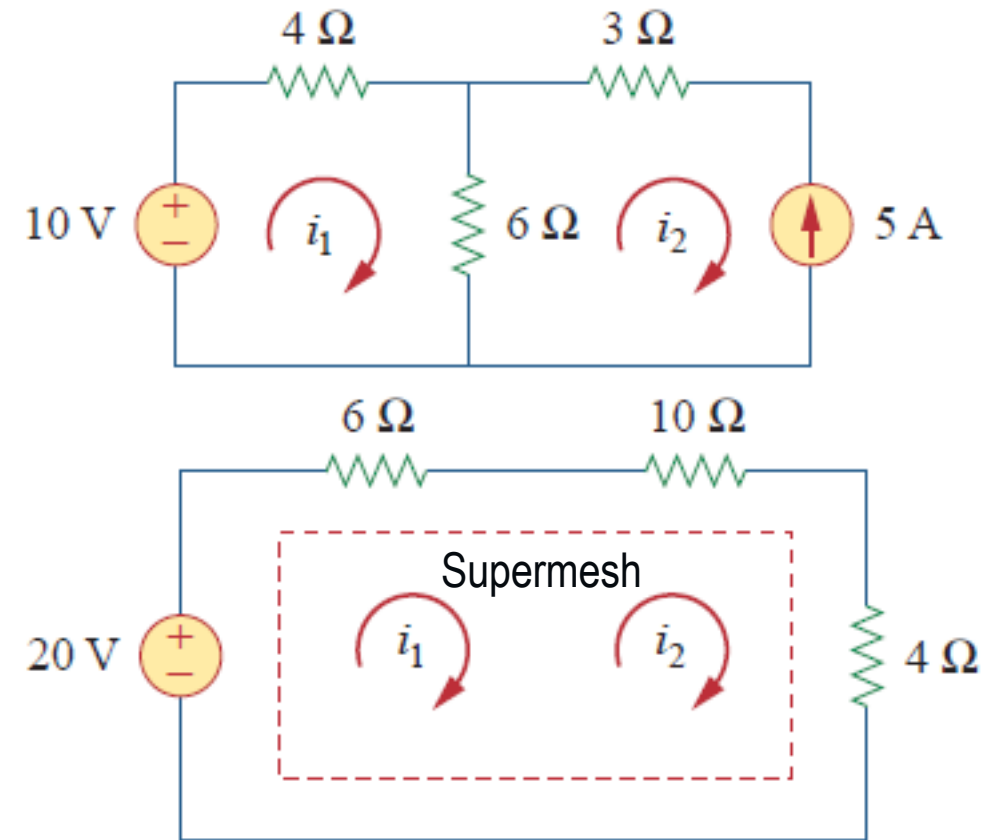
□ CASE 1 → Current source in one mesh

$$i_2 = -5 \text{ A}, \quad -10 + 4i_1 + 6(i_1 - i_2) = 0 \rightarrow i_1 = -2 \text{ A}$$

□ CASE 2 → Common current source in two meshes



$$-20 + 6i_1 + 10i_2 + 4i_2 = 0, \quad i_2 - i_1 = 6 \rightarrow i_1 = -3,2 \text{ A}, \quad i_2 = 2.8 \text{ A}$$



## WHICH ONE IS BETTER...

THE LESS EQUATIONS → THE EASIER SOLUTION



### Advice-1

- Mesh analysis
  - Many series elements, voltage sources, supermeshes, fewer meshes than nodals
- Nodal analysis
  - Many parallel elements, current sources, supernodes, fewer nodals than meshes

### Advice-2

- Nodal analysis
  - Nodal voltages required
- Mesh analysis
  - Branch / mesh currents required





- Nodal Analysis
- Mesh Analysis
- Applications (*DC Transistor Circuits*)**

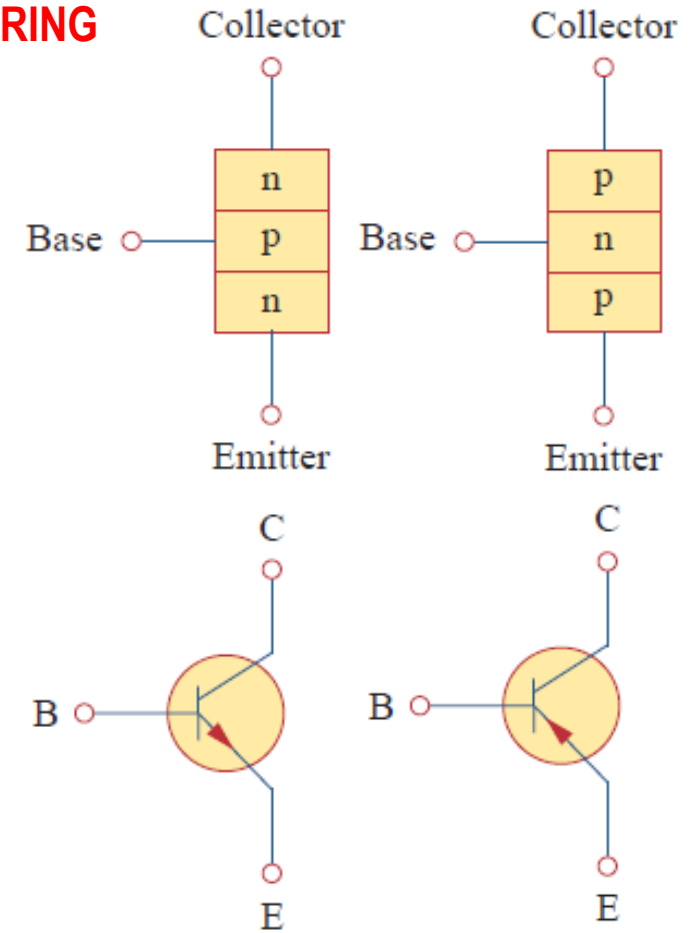
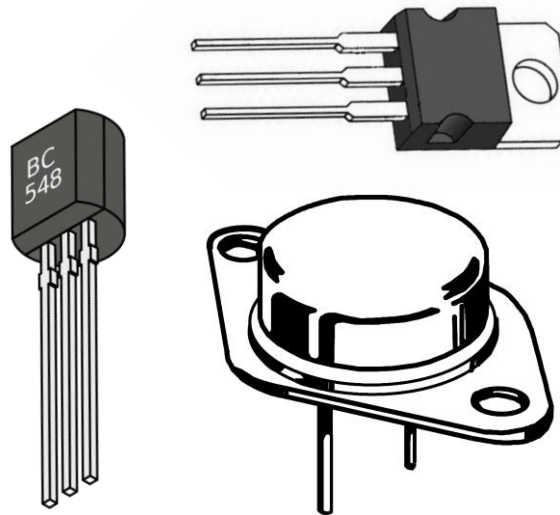
# Applications: DC Transistor Circuits



## INDUSTRIAL AGE → AGE OF THE ENGINEERING

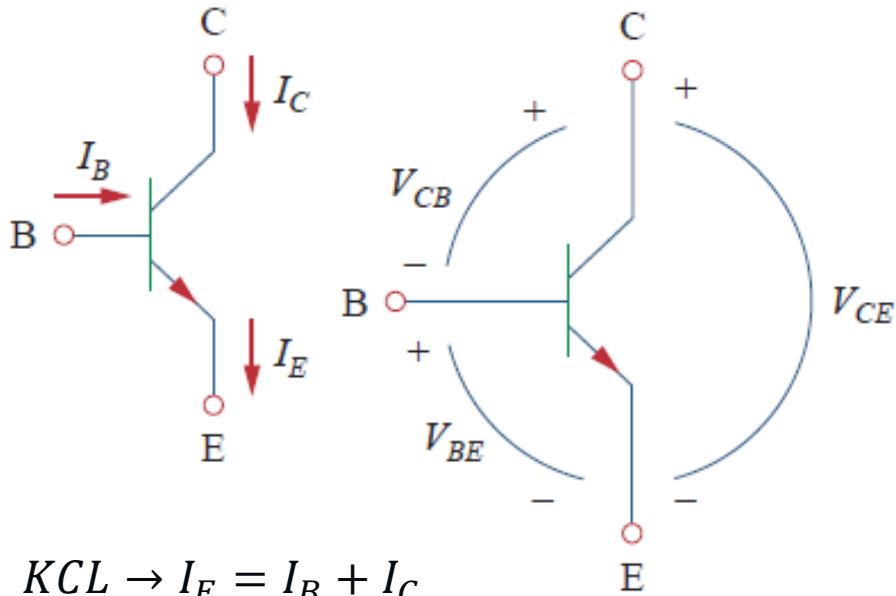
### Bell Labs

- ❑ Bardeen, Brattain ('47) point contact trans.
- ❑ Shockley ('48) bip. junct. transistor (BJT)
- ❑ Shockley ('54) FET (widely used today)
- ❑ Nobel Prize in Physics ('56) for 3 inventors



# Transistor Model

Transistor → current dependent current source



$$KCL \rightarrow I_E = I_B + I_C$$

$$KVL \rightarrow V_{CE} = V_{BE} + V_{BC}$$

Characteristic properties

Common-base current gain

$$(\alpha) \rightarrow I_C = \alpha I_E, \quad \alpha \approx 0.99$$

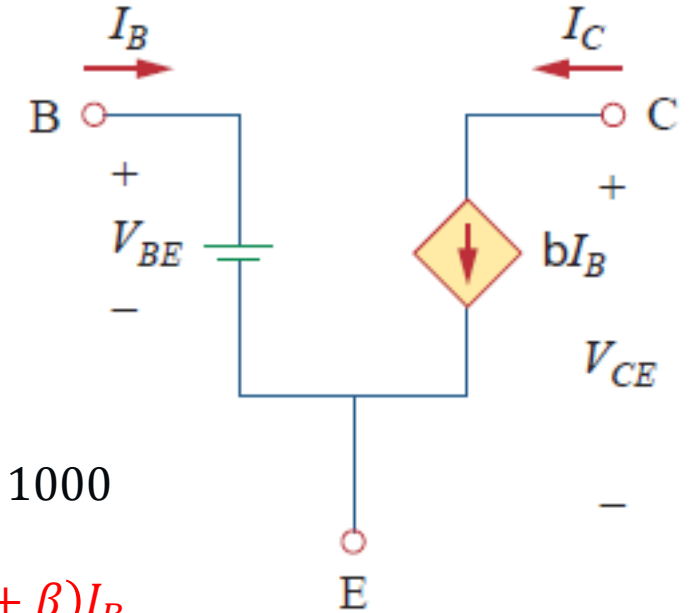
Common-emitter current gain

$$(\beta) \rightarrow I_C = \beta I_B, \quad \beta \approx 50 \dots 1000$$

$$I_E = I_B + I_C = I_B + \beta I_B = (1 + \beta) I_B$$

$$\beta = \frac{I_C}{I_B} = \frac{\alpha I_E}{I_E - I_C} = \frac{\alpha I_E}{I_E - \alpha I_E} = \frac{\alpha}{1 - \alpha}$$

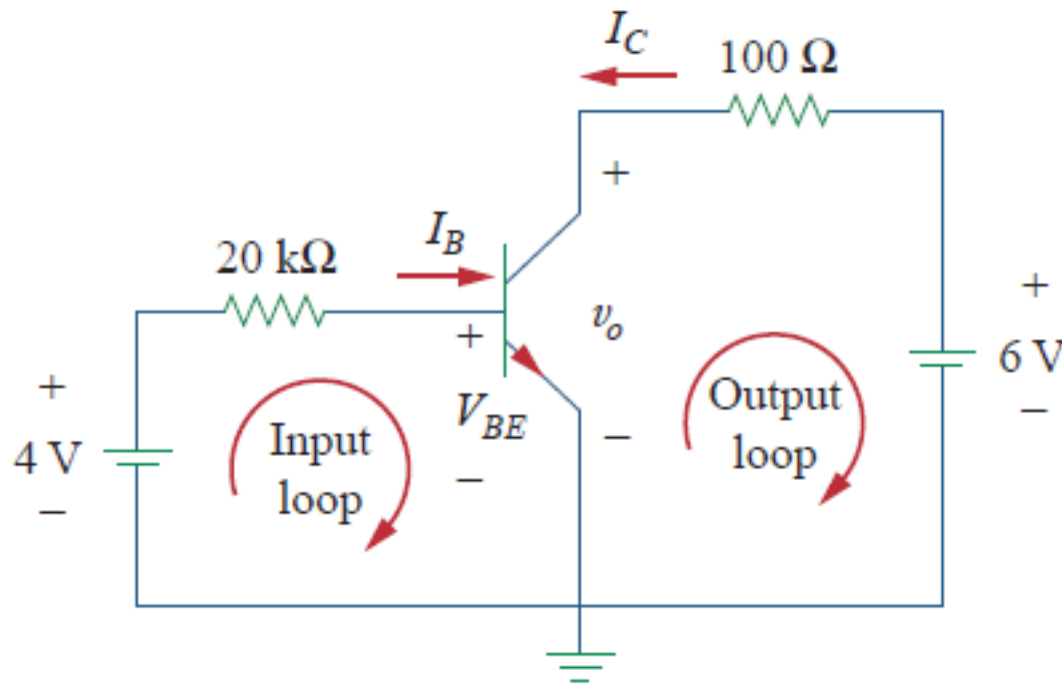
Active mode  
→  $V_{BE} \approx 0.7 V$



Operation modes → [active], [cutoff], [saturation]

## Example with DC Transistor Circuits

Find  $I_B$ ,  $I_C$ ,  $v_o$  if  $\beta = 50$  (transistor operates in active mode)



$$\text{Input loop: } -4 + I_B \cdot 20 \cdot 10^3 + V_{BE} = 0$$

$$V_{BE} = 0.7 \rightarrow I_B = \frac{4 - 0.7}{20 \cdot 10^3} = 165 \mu\text{A}$$

$$I_C = \beta \cdot I_B = 50 \cdot 165 \mu\text{A} = 8.25 \text{ mA}$$

$$\text{Output loop: } -v_o - 100I_C + 6 = 0$$

$$v_o = 6 - 100I_C = 6 - 0.825 = 5.175 \text{ V}$$

