



DR. GYURCSEK ISTVÁN

Operational Amplifiers

Sources and additional materials (recommended)

- ❑ *Dr. Gyurcsek – Dr. Elmer: Theories in Electric Circuits, GlobeEdit, 2016, ISBN:978-3-330-71341-3*
- ❑ *Ch. Alexander, M. Sadiku: Fundamentals of Electric Circuits, 6th Ed., McGraw Hill NY 2016, ISBN: 978-0078028229*
- ❑ *Simonyi K.: Villamosságtan. AK Budapest 1983, ISBN:9630534134*
- ❑ *Dr. Selmeczi K. – Schnöller A.: Villamosságtan 1. MK Budapest 2002, TK szám: 49203/I*
- ❑ *Dr. Selmeczi K. – Schnöller A.: Villamosságtan 2. TK Budapest 2002, ISBN:9631026043*
- ❑ *Zombory L.: Elektromágneses terek. MK Budapest 2006, (www.electro.uni-miskolc.hu)*



- Operation Amplifier**
- Op Amp Circuits
- Applications

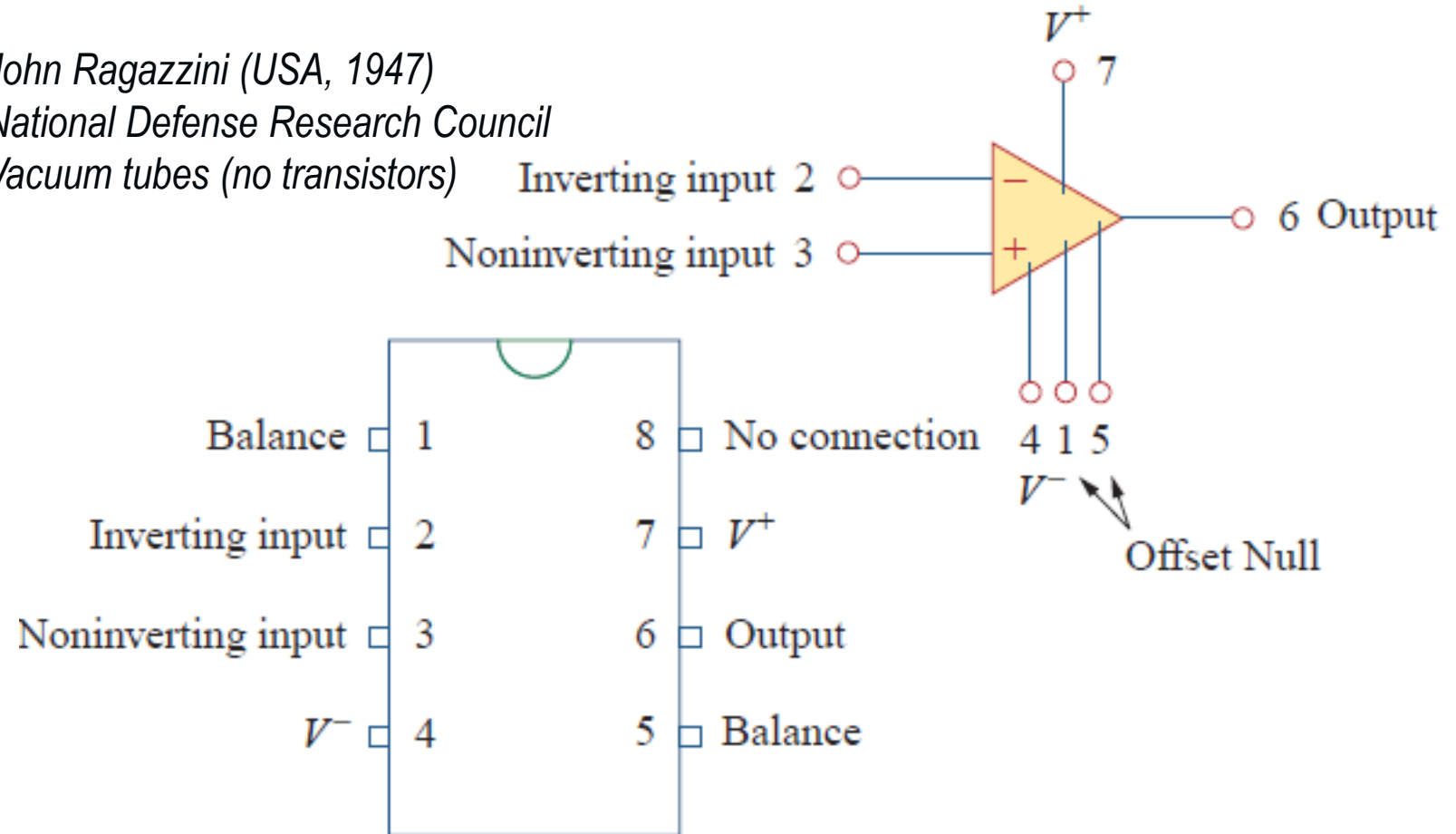
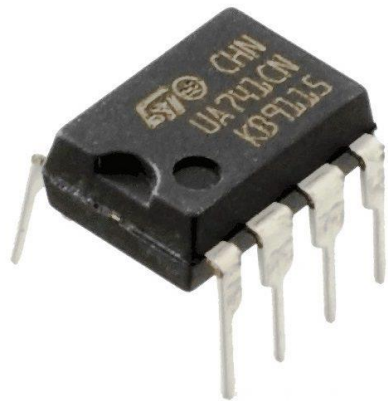
Introduction



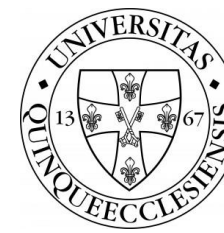
OP AMP = [BUILDING BLOCK], [V-CONTROLLED V-SOURCE], [MATHS ,OPS']



John Ragazzini (USA, 1947)
National Defense Research Council
Vacuum tubes (no transistors)



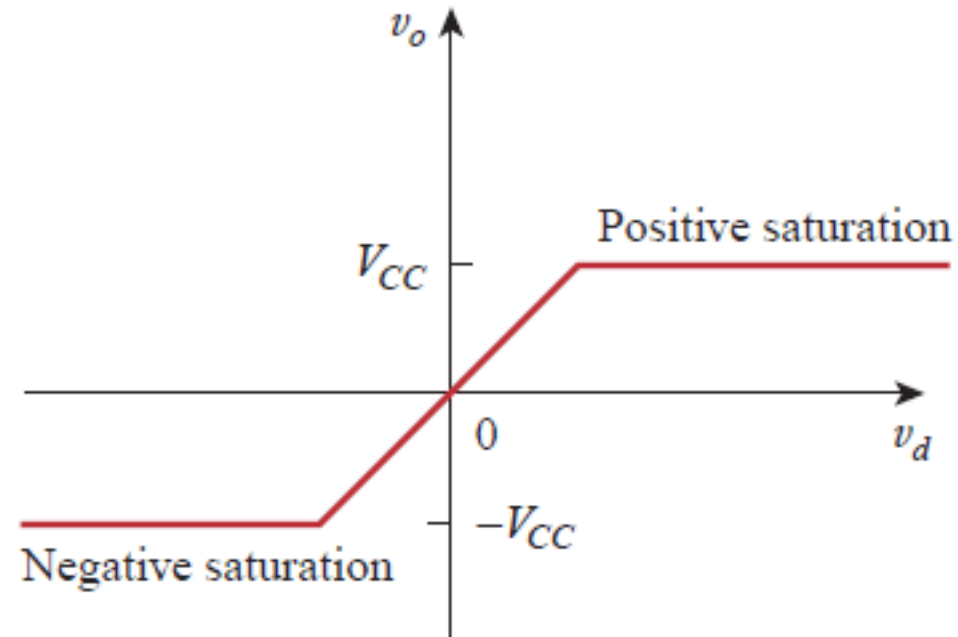
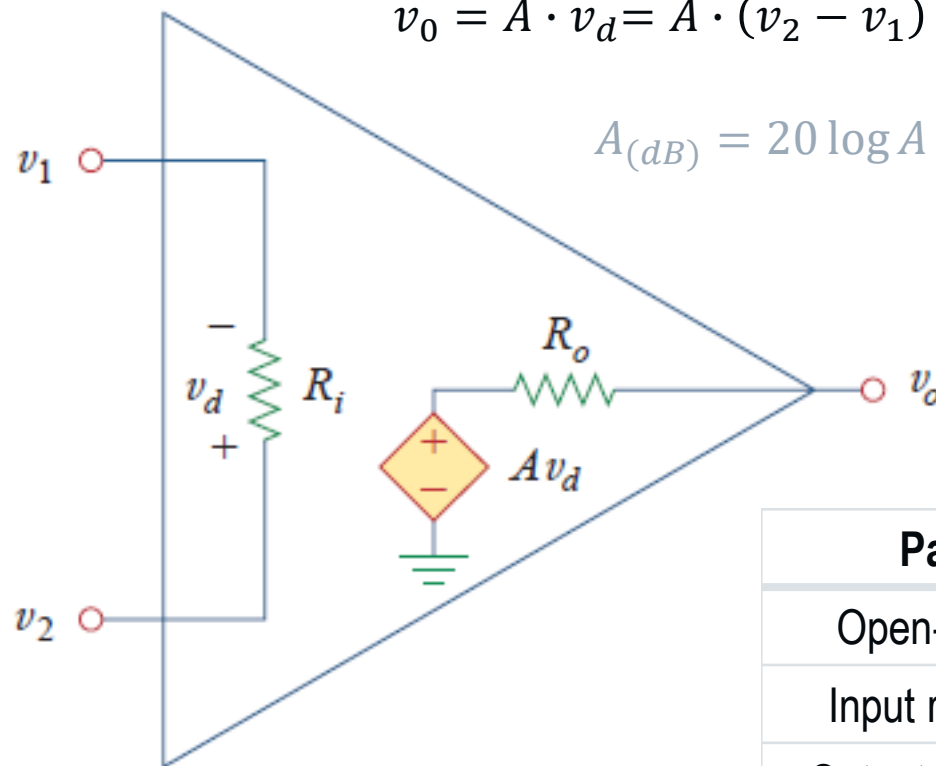
Equivalent Circuit



$A \rightarrow$ open loop (no feedback) voltage gain

$$v_o = A \cdot v_d = A \cdot (v_2 - v_1)$$

$$A_{(dB)} = 20 \log A$$

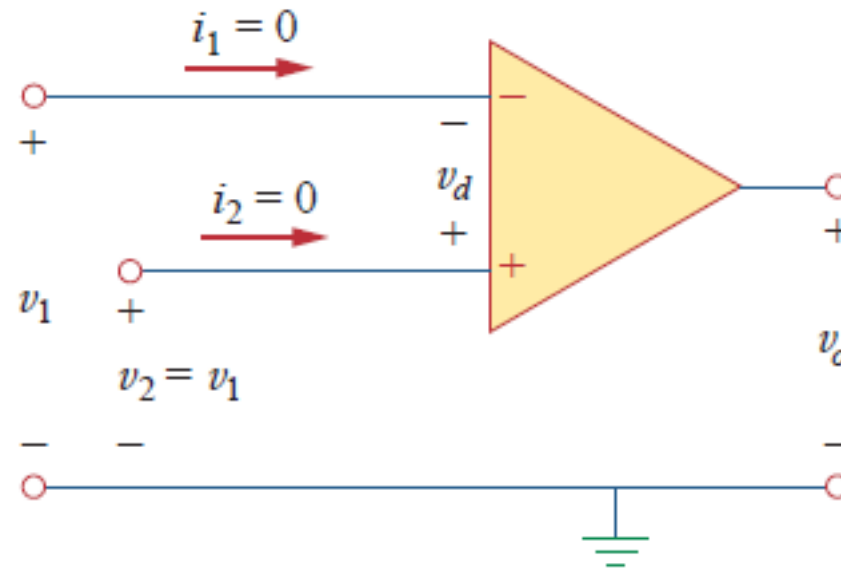


Parameter	Ideal value	Typical range
Open-loop gain, A	∞	10^5 - 10^8 (100-160 dB)
Input resistance, R_i	$\infty \Omega$	$10^5 - 10^{13} \Omega$
Output resistance, R_o	0Ω	10 – 100 Ω
Supply voltage, V_{CC}		5 – 24 V

Ideal Op Amp



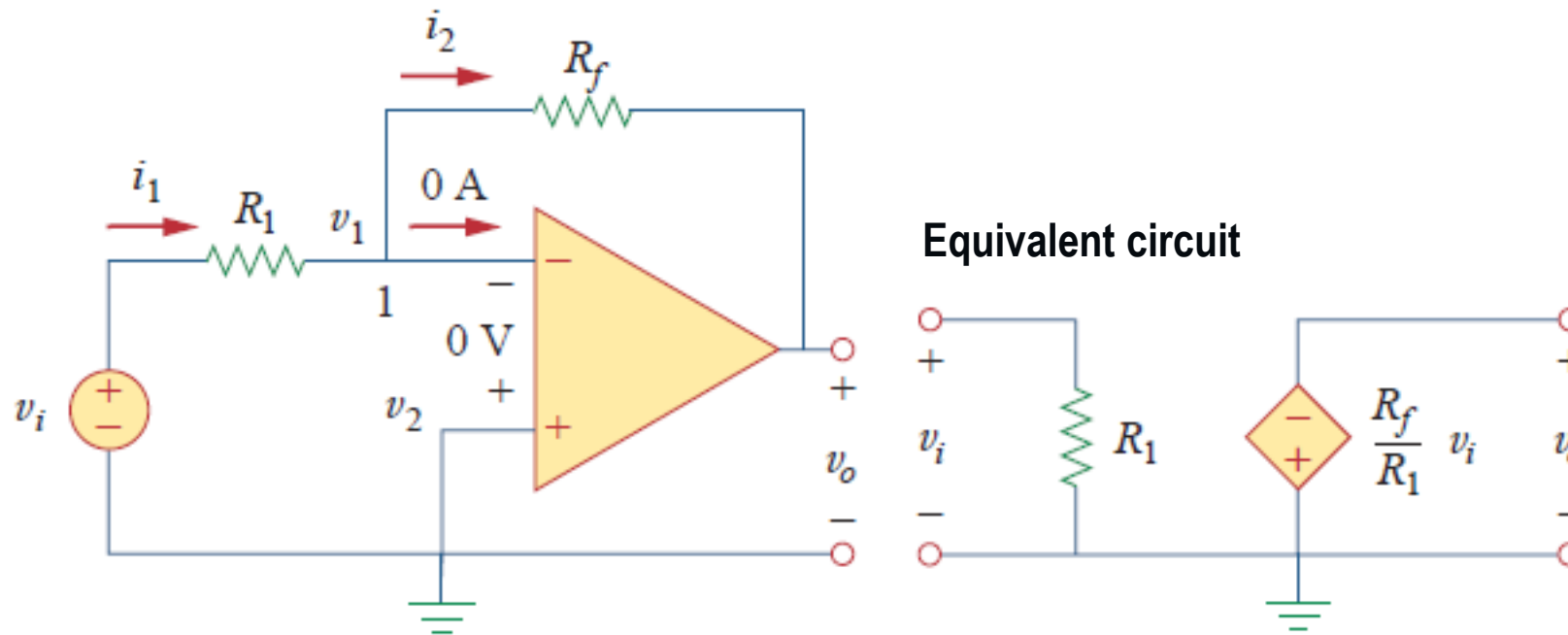
$$\left. \begin{array}{l} A \cong \infty \\ R_i = \infty \\ R_o = 0 \end{array} \right\} \rightarrow \left\{ \begin{array}{l} i_1 = 0 \\ i_2 = 0 \\ v_1 = v_2 \end{array} \right.$$





- ❑ Operation Amplifier
- ❑ **Op Amp Circuits**
- ❑ Applications

Inverting Amplifier



$$i_1 = i_2 \rightarrow \frac{v_i - v_1}{R_1} = \frac{v_1 - v_0}{R_f}$$

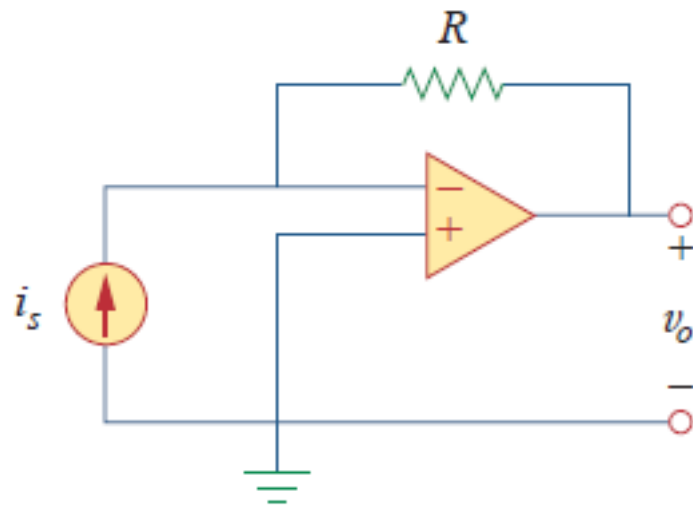
$$v_1 = v_2 = 0 \rightarrow \frac{v_i}{R_1} = -\frac{v_0}{R_f}$$

$$v_0 = -\frac{R_f}{R_1} v_i \leftarrow \text{reverses the polarity}$$

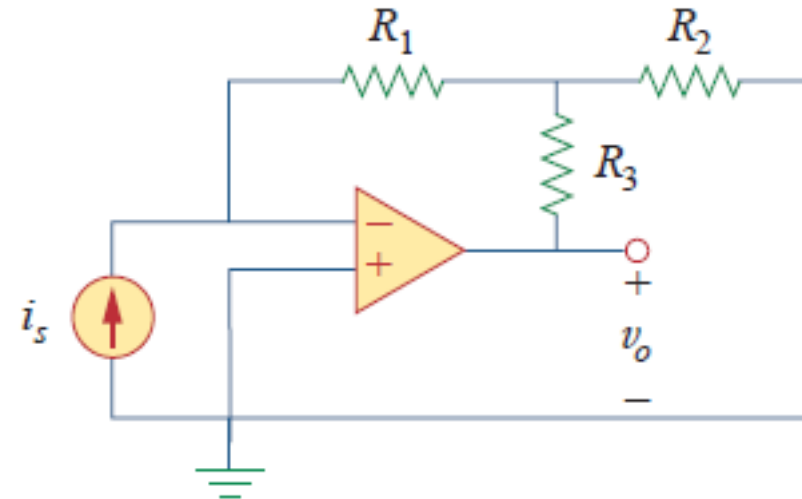
Current-to-Voltage Converters



HW – Show the followings...

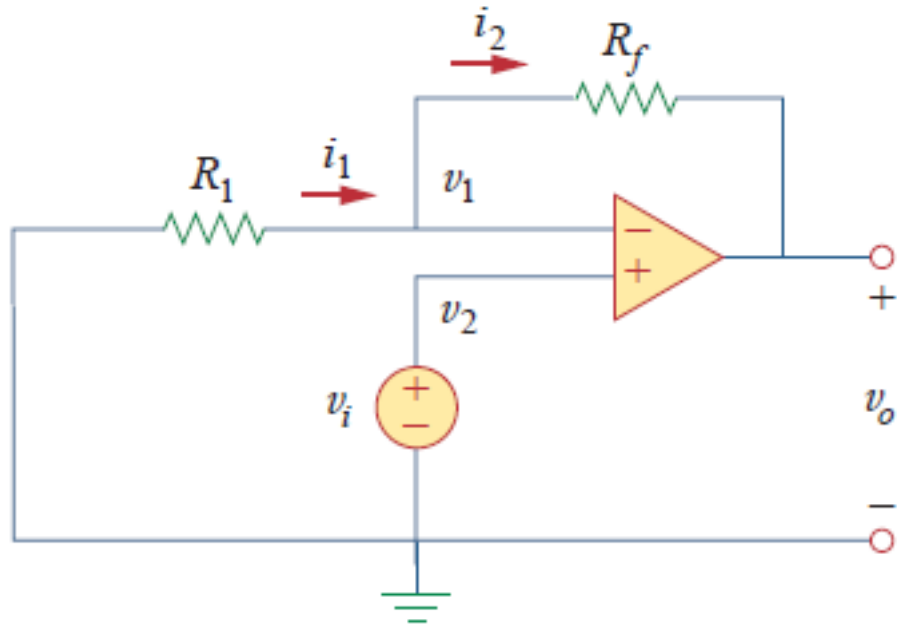
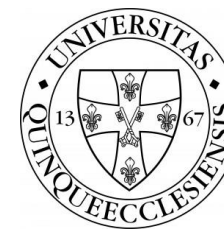


$$\frac{v_o}{i_s} = -R$$



$$\frac{v_o}{i_s} = -R_1 \left(1 + \frac{R_3}{R_1} + \frac{R_3}{R_2} \right)$$

Noninverting Amplifier

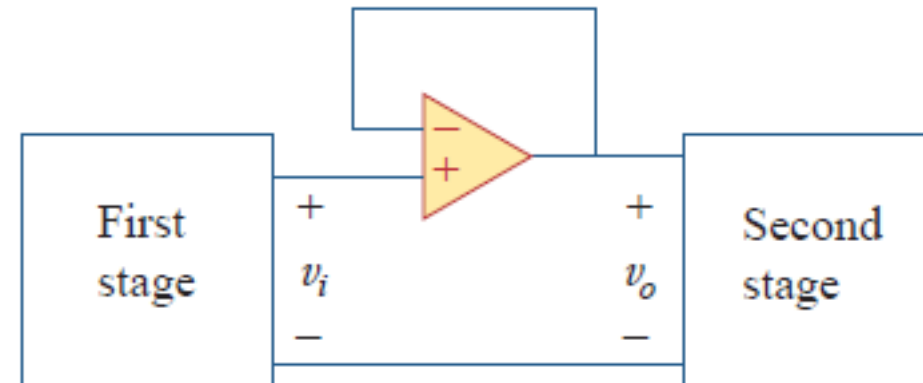
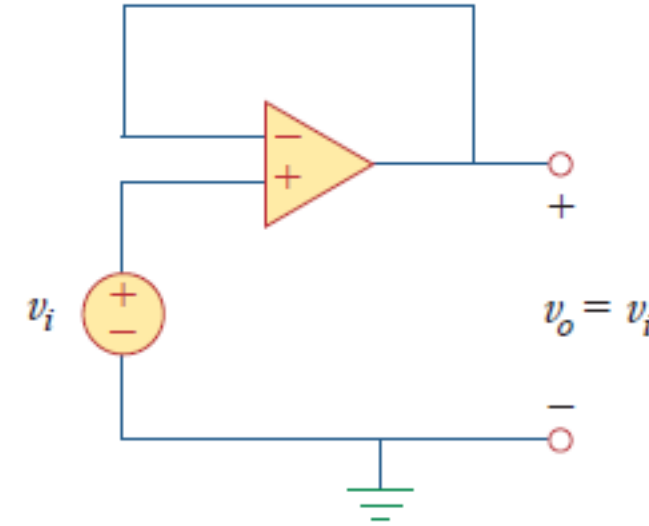


$$i_1 = i_2 \rightarrow \frac{0 - v_1}{R_1} = \frac{v_1 - v_o}{R_f}$$

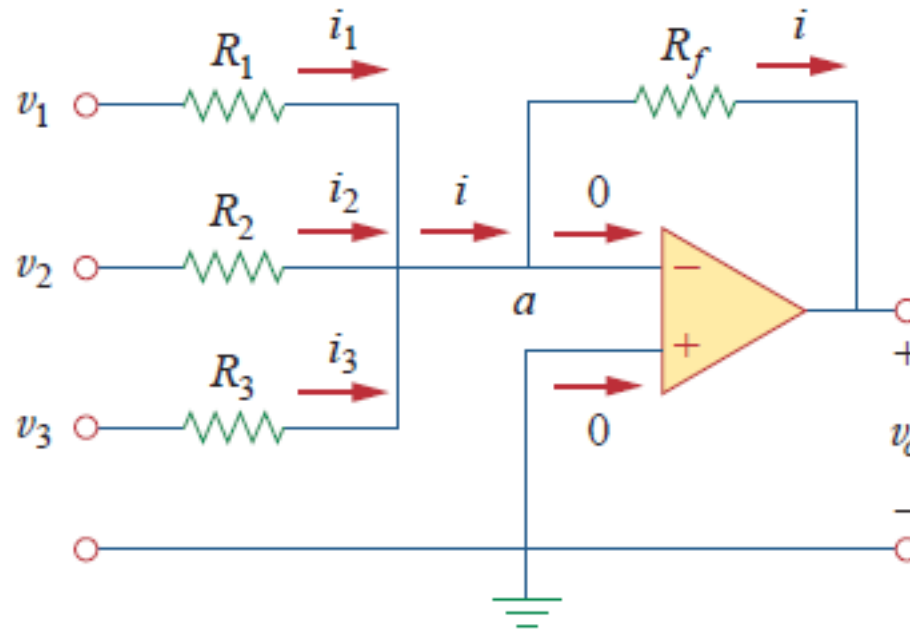
$$v_1 = v_2 = v_i \rightarrow \frac{-v_i}{R_1} = \frac{v_i - v_o}{R_f}$$

$$v_o = \left(1 + \frac{R_f}{R_1}\right) v_i \quad A_v = \frac{v_o}{v_i} = 1 + \frac{R_f}{R_1} > 0$$

Voltage follower – to isolate two cascaded stages



Summing Amplifier (Weighted!)



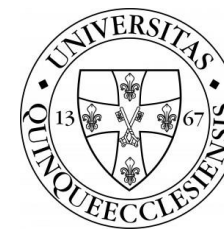
$$(1): i = i_1 + i_2 + i_3$$

$$(2): v_a = 0$$

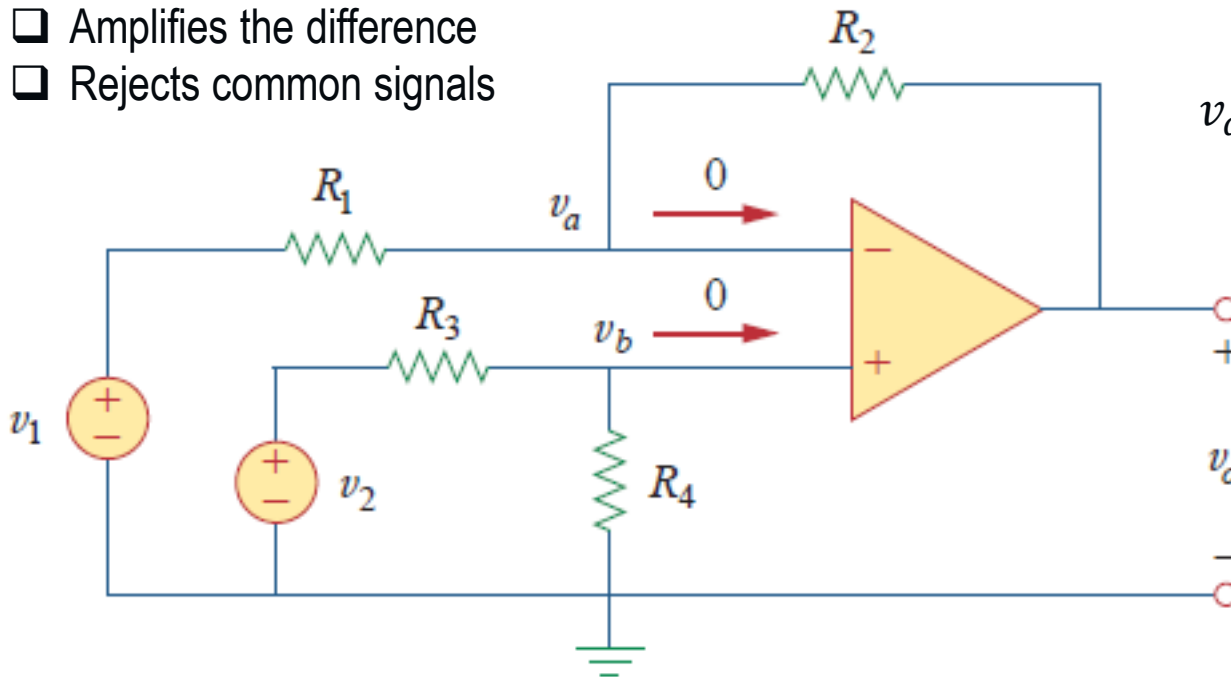
$$(3): i_1 = \frac{v_1 - v_a}{R_1}, \quad i_2 = \frac{v_2 - v_a}{R_2}, \quad i_3 = \frac{v_3 - v_a}{R_3}, \quad i = \frac{v_a - v_o}{R_f}$$

$$(2)(3) \rightarrow (1): \frac{0 - v_o}{R_f} = \frac{v_1 - 0}{R_1} + \frac{v_2 - 0}{R_2} + \frac{v_3 - 0}{R_3} \rightarrow v_o = - \left(\frac{R_f}{R_1} v_1 + \frac{R_f}{R_2} v_2 + \frac{R_f}{R_3} v_3 \right)$$

Differential Amplifier



- ❑ Amplifies the difference
- ❑ Rejects common signals



$$v_a = v_b, (\mathbf{b} \rightarrow \mathbf{a}): v_0 = v_2 \left(1 + \frac{R_2}{R_1} \right) \frac{R_4}{R_3 + R_4} - v_1 \frac{R_2}{R_1}$$

$$v_0 = v_2 \frac{R_2 \left(1 + \frac{R_1}{R_2} \right)}{R_1 \left(1 + \frac{R_3}{R_4} \right)} - v_1 \frac{R_2}{R_1}$$

- ❑ ,very high' Common Mode Rejection (CMR) when

$$\frac{R_1}{R_2} = \frac{R_3}{R_4} \rightarrow v_0 = \frac{R_2}{R_1} (v_2 - v_1)$$

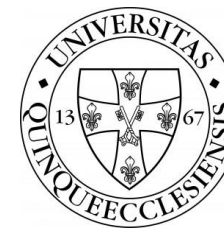
- ❑ ,Subtractor' when

$$R_1 = R_2, R_3 = R_4 \rightarrow v_0 = v_2 - v_1$$

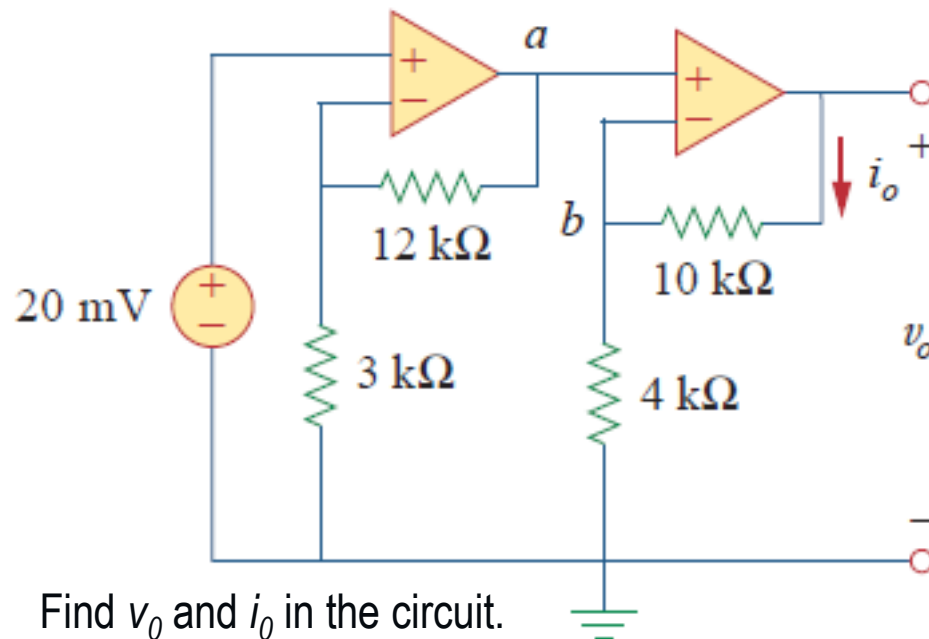
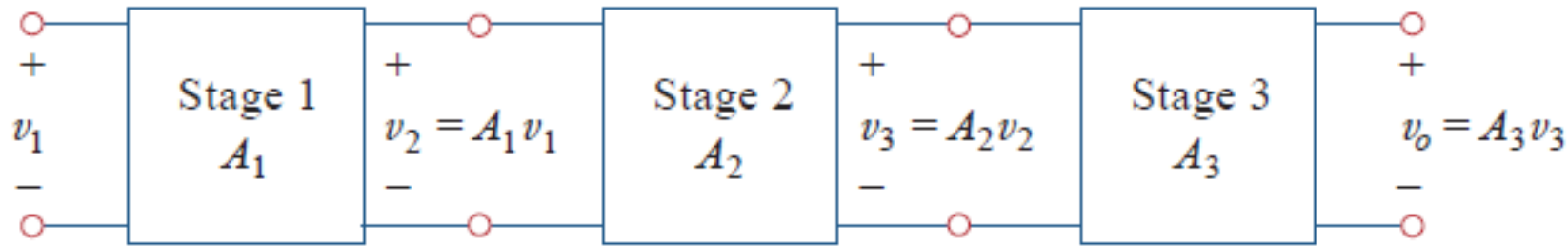
$$(\mathbf{node\ a}): \frac{v_1 - v_a}{R_1} = \frac{v_a - v_0}{R_2} \rightarrow v_0 = v_a \left(1 + \frac{R_2}{R_1} \right) - v_1 \frac{R_2}{R_1}$$

$$(\mathbf{node\ b}): \frac{v_2 - v_b}{R_3} = \frac{v_b - 0}{R_4} \rightarrow v_b = v_2 \frac{R_4}{R_3 + R_4}$$

Cascaded Op Amps



Cascade connection → 'head-to-tail arrangement' [output of one] → [input of the next].



$$A = A_1 \cdot A_2 \cdot A_3$$

$$v_a = \left(1 + \frac{12}{3}\right) \cdot 20 = 100 \text{ mV}$$

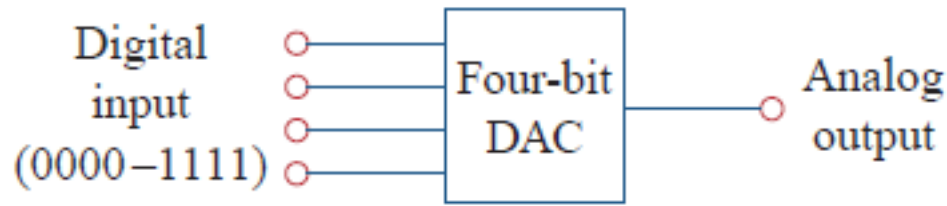
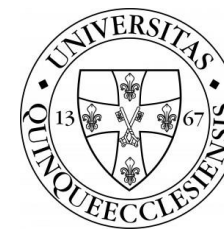
$$v_0 = \left(1 + \frac{10}{4}\right) \cdot v_a = 350 \text{ mV}$$

$$v_b = v_a \rightarrow i_0 = \frac{v_0 - v_b}{10k} = \frac{250}{10} = 25 \mu\text{A}$$



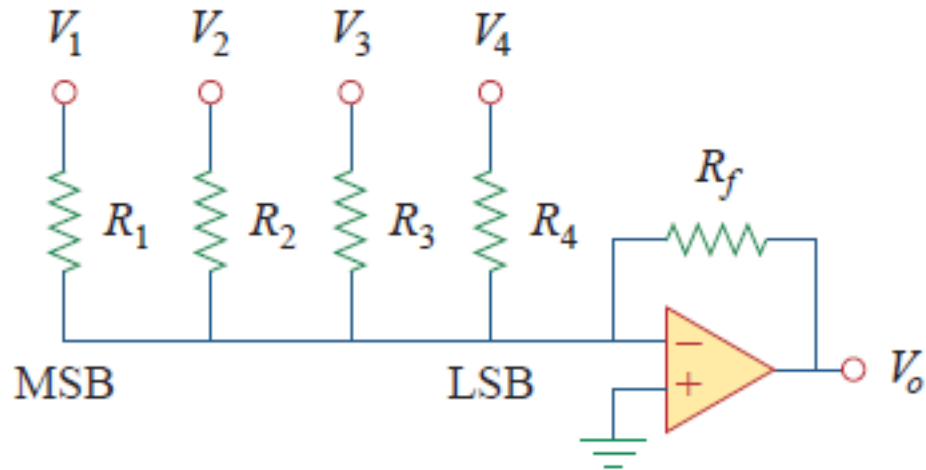
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DA Converter



$$-V_0 = \frac{R_f}{R_1} V_1 + \frac{R_f}{R_2} V_2 + \frac{R_f}{R_3} V_3 + \frac{R_f}{R_4} V_4$$

Example $R_f = 2k$, $R_1 = 10k$, $R_2 = 20k$, $R_3 = 40k$, $R_4 = 80k$
 Find analog output(s) for [0000], [0001], [0010], ..., [1111]



$$-V_0^{(0000)} = \frac{2k}{10k} \cdot 0 + \frac{2k}{20k} \cdot 0 + \frac{2k}{40k} \cdot 0 + \frac{2k}{80k} \cdot 0 = 0 \text{ V}$$

$$-V_0^{(0001)} = \frac{2k}{10k} \cdot 0 + \frac{2k}{20k} \cdot 0 + \frac{2k}{40k} \cdot 0 + \frac{2k}{80k} \cdot (5V) = 125 \text{ mV}$$

$$-V_0^{(0011)} = \frac{2k}{10k} \cdot 0 + \frac{2k}{20k} \cdot 0 + \frac{2k}{40k} \cdot (5V) + \frac{2k}{80k} \cdot (5V) = 375 \text{ mV}$$

$$-V_0^{(1111)} = \frac{2k}{10k} \cdot (5V) + \frac{2k}{20k} \cdot (5V) + \frac{2k}{40k} \cdot (5V) + \frac{2k}{80k} \cdot (5V) = 1.875 \text{ V}$$

Binary weighted ladder

(V_1 - MSB: Most Significant Bit)

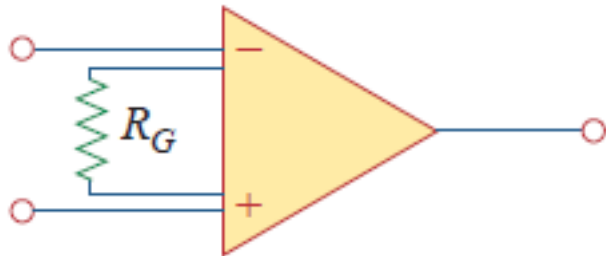
(V_4 - LSB: Least Significant Bit)

Instrumentation Amplifier



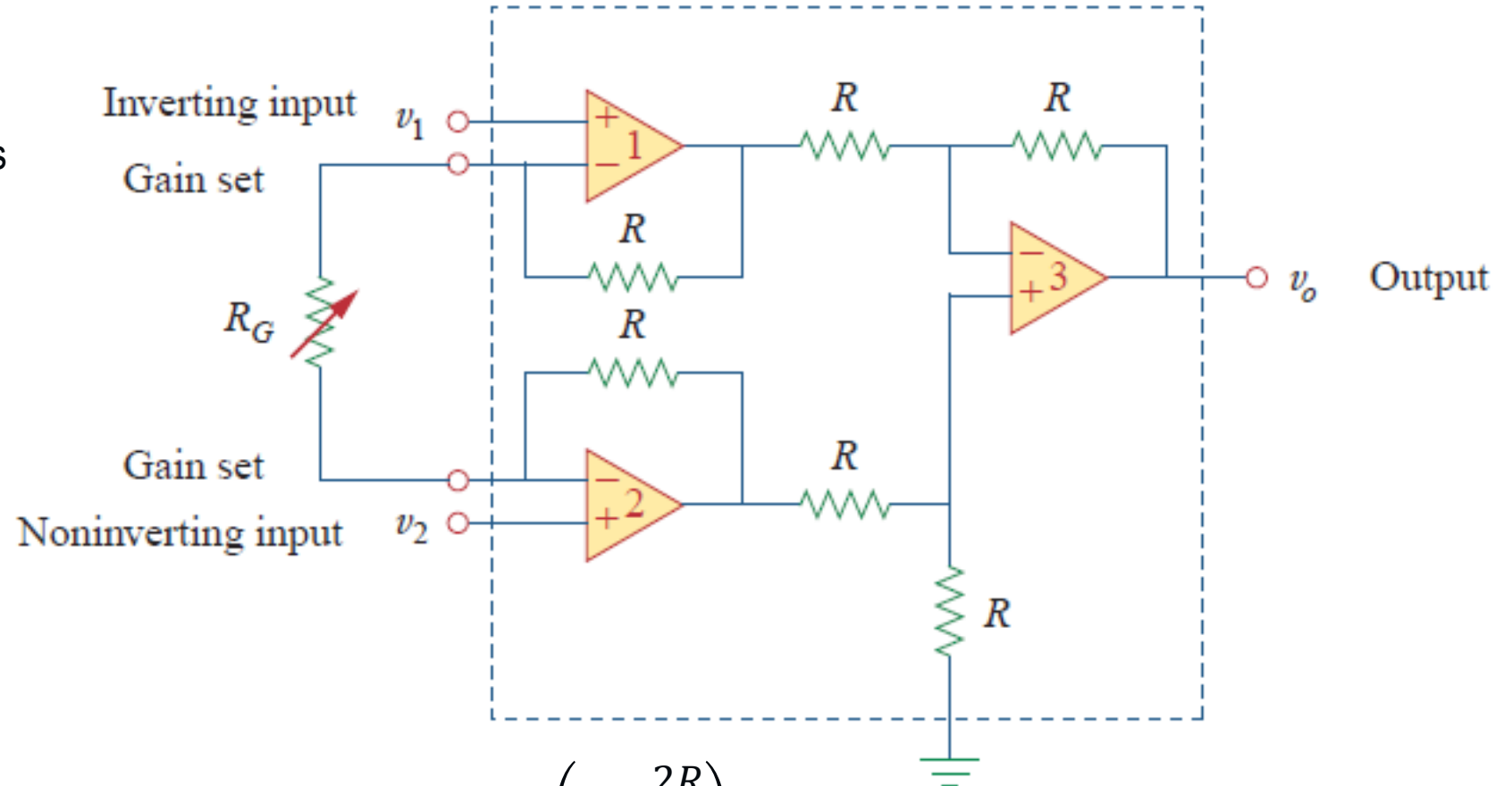
IA – [mérőerősítő]

- Extension of the difference amplifier
- Consists of three op amps + resistors
- External R_G for gain adjustment



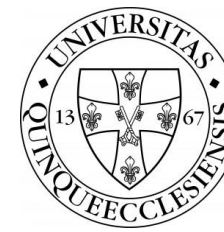
Widely used

- Precision measurement
- Process control
- Data acquisition systems.
- Isolation amplifiers
- Thermo couple amplifiers



$$v_0 = A_v(v_2 - v_1), \quad A_v = \left(1 + \frac{2R}{R_G}\right)$$

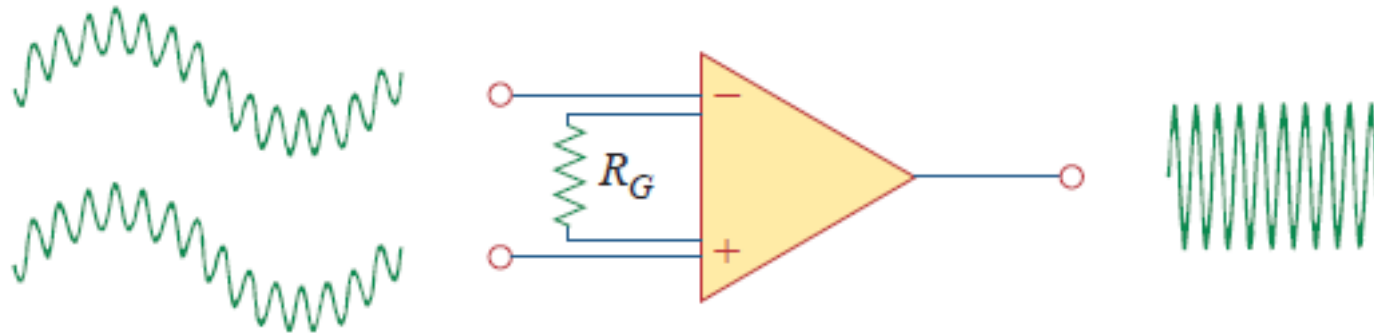
Instrumentation Amplifier



Small differential signals riding on larger common-mode signals

$$v_0 = A_v(v_2 - v_1)$$

Amplified differential signal
No common-mode signal



,IA' characteristics

- Gain is adjusted by *one* external resistor R_G .
- Gain independent and very high input impedances
- Very high CMR (common mode rejection)

Single-package units

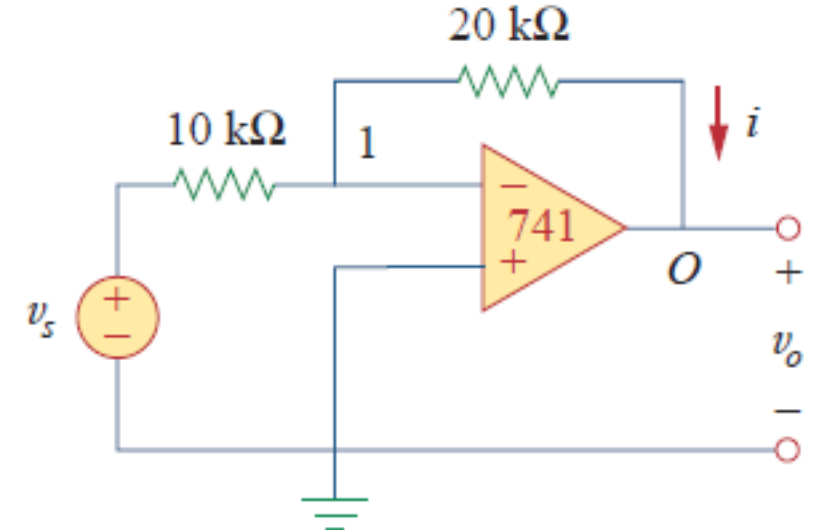
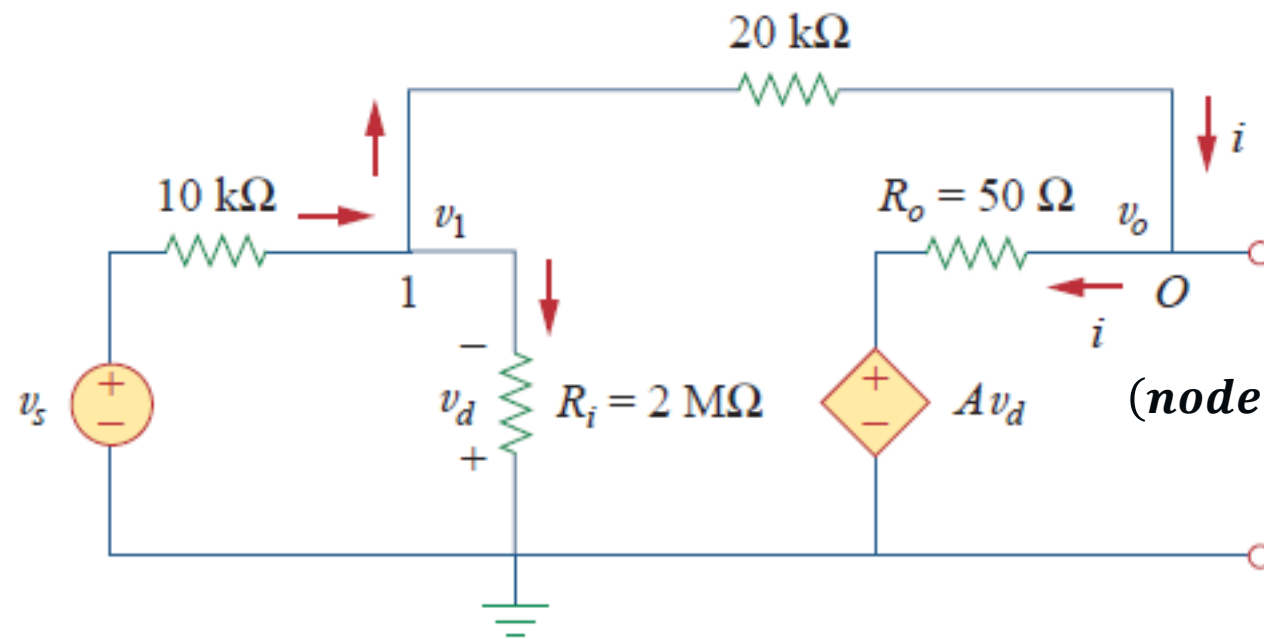
- LH0036 (*National Semiconductor*)
- Gain ...1 - 1,000 by external R_G
(R_G ... 100 - 10 k)

Non-Ideal Op Amp Example.1



$A = 2 \cdot 10^5$, $R_i = 2 \text{ M}\Omega$, $R_o = 50 \Omega$. Find the closed-loop gain (v_o/v_s) and i when $v_s = 2 \text{ V}$.

Solution (equivalent circuit)

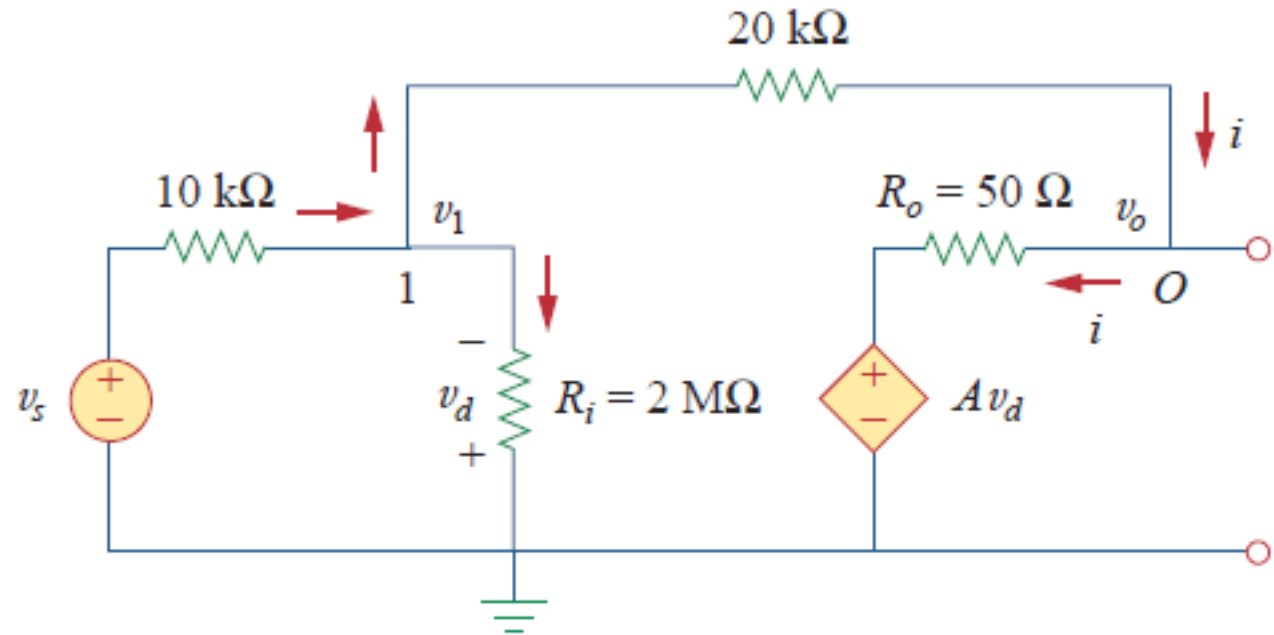
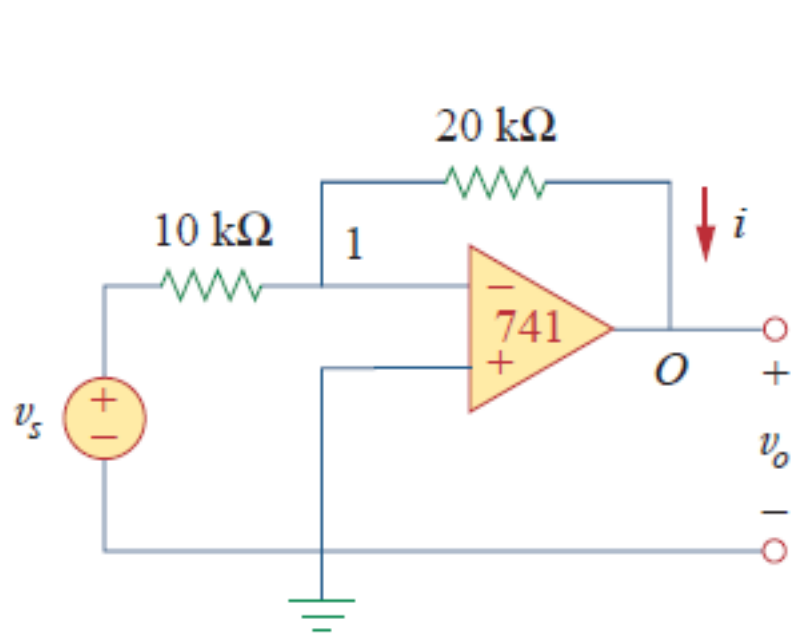


$$\text{(node 1): } \frac{v_s - v_1}{10 \cdot 10^3} = \frac{v_1}{2 \cdot 10^6} + \frac{v_1 - v_o}{20 \cdot 10^3} \rightarrow \text{(1): } v_1 = \frac{2v_s + v_o}{3}$$

$$\text{(node O): } \frac{v_1 - v_o}{20 \cdot 10^3} = \frac{v_o - Av_d}{50}, v_d = -v_1$$

$$\text{(2): } v_1 - v_o = 400(v_o + 200,000v_1)$$

Non-Ideal Op Amp Example.1



$$(1): v_1 = \frac{2v_s + v_o}{3}$$

$$(2): v_1 - v_o = 400(v_o + 200,000v_1)$$

$$(1) \rightarrow (2): 0 \cong 26,667,067v_o + 53,333,333v_s \rightarrow \frac{v_o}{v_s} = -1.9999$$

$$v_s = 2 \rightarrow v_o = 3.9999398 V$$

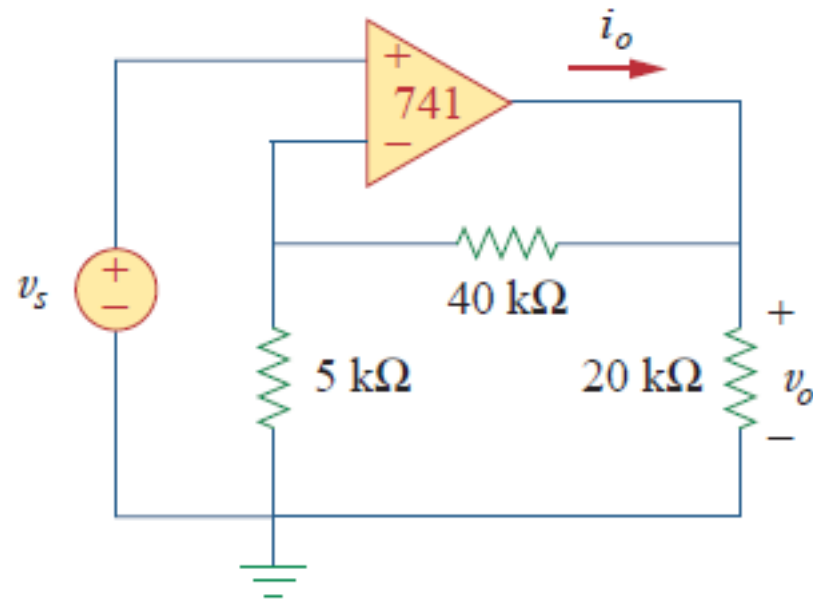
$$v_1 = 20.066667 \mu V$$

$$i = \frac{v_1 - v_o}{20 \cdot 10^3} = 199.99 \mu A$$

Non-Ideal Op Amp Example.2



$A = 2 \cdot 10^5$, $R_i = 2 \text{ M}\Omega$, $R_o = 50 \Omega$. Calculate the closed-loop gain (v_o/v_s) and i_o when $v_s = 1\text{V}$.



Solution (9.00041, 0.657 mA.)

Questions

