



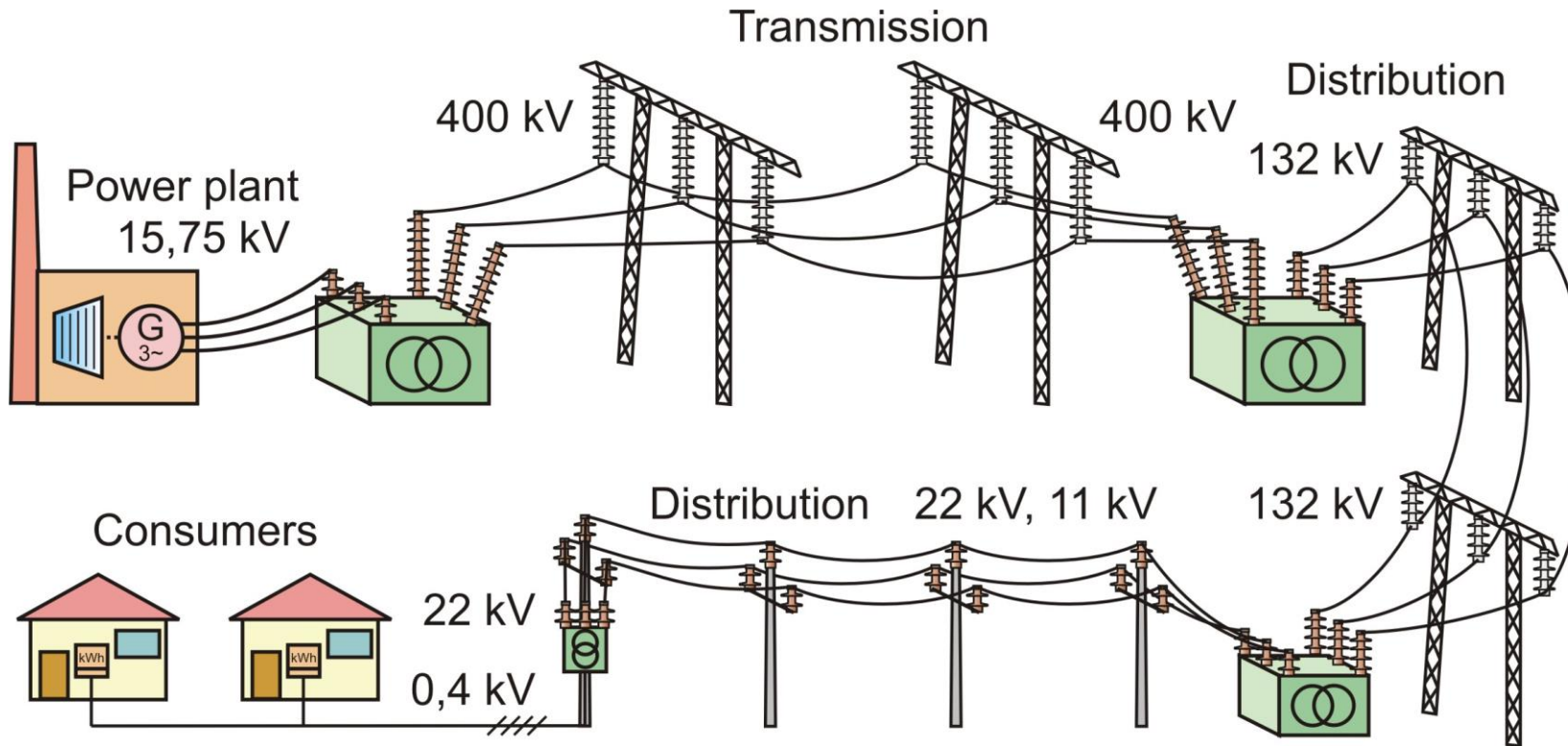
DR. GYURCSEK ISTVÁN

# Three-Phase Circuits

## *Sources and additional materials (recommended)*

- ❑ *Dr. Gyurcsek – Dr. Elmer: Theories in Electric Circuits, GlobeEdit, 2016, ISBN:978-3-330-71341-3*
- ❑ *Ch. Alexander, M. Sadiku: Fundamentals of Electric Circuits, 6th Ed., McGraw Hill NY 2016, ISBN: 978-0078028229*
- ❑ *Fleckenstein: Three-Phase Electrical Power (ISBN-13: 978-1498737777)*
- ❑ *Delmar: 3-phase Circuits and Electrical Machines (ISBN-13: 978-1439059821)*
- ❑ *Mayergoyz - Lawson: Basic Electric Circuit Theory (ISBN13: 978-0124808652)*
- ❑ *Simonyi K.: Villamosságtan. AK Budapest 1983, ISBN:9630534134*

# Generation, Transmission, Distribution

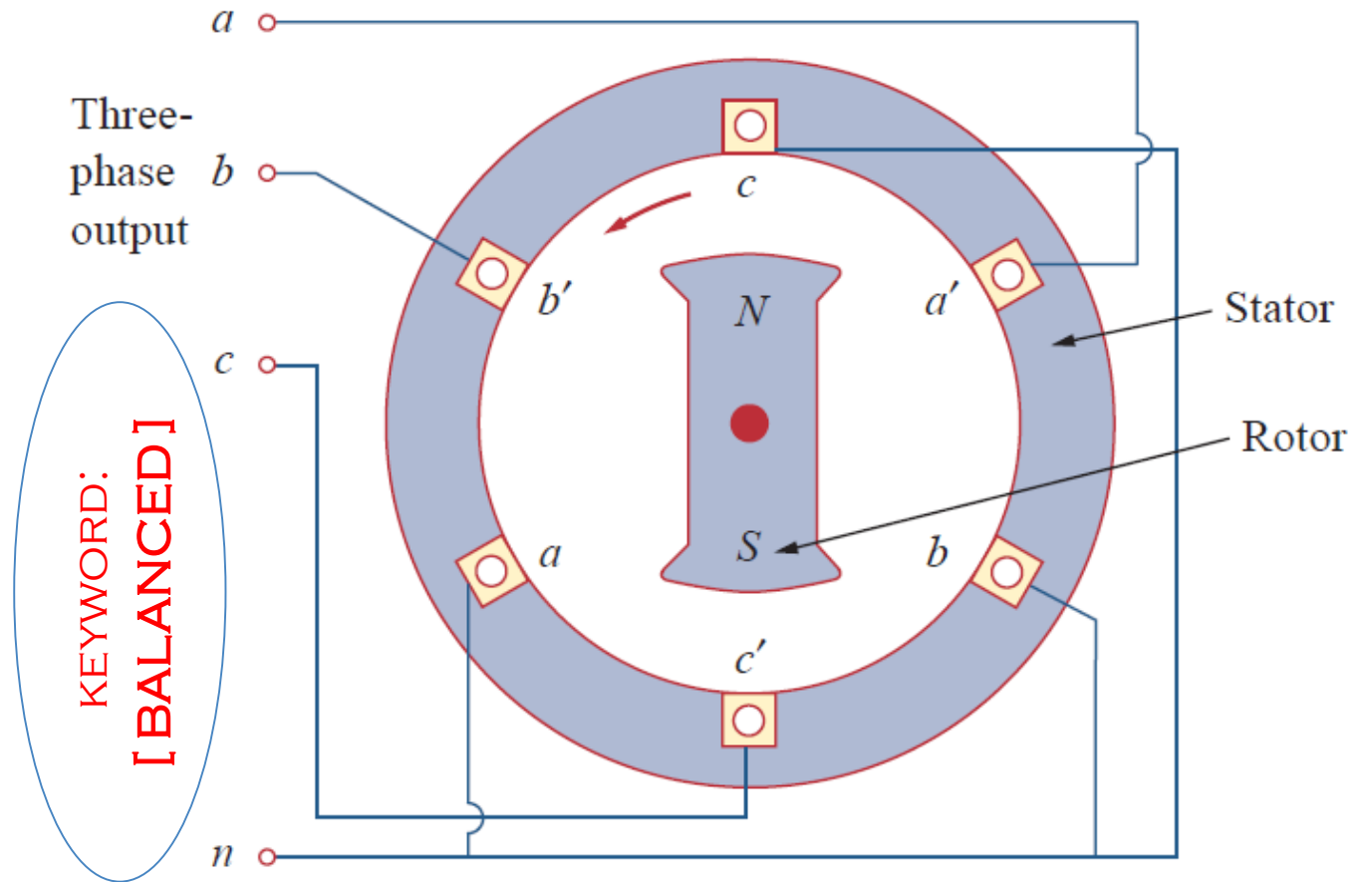
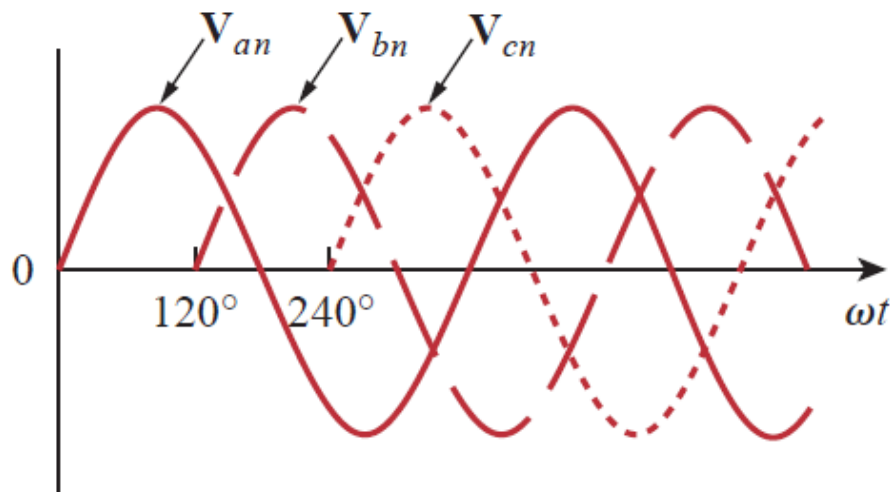


# Why Three-Phase... ?



*‘Three-phase power is the most efficient way that electricity could be produced, transmitted, consumed.’*

- ❑ Single-phase power → falls to zero three times
- ❑ Three-phase power → never falls to zero
- ❑ Delivered power is the same at any instant
- ❑ Motors / transformers → 150% operating charact.
- ❑ 33% save in mass of conductors (*see later*)

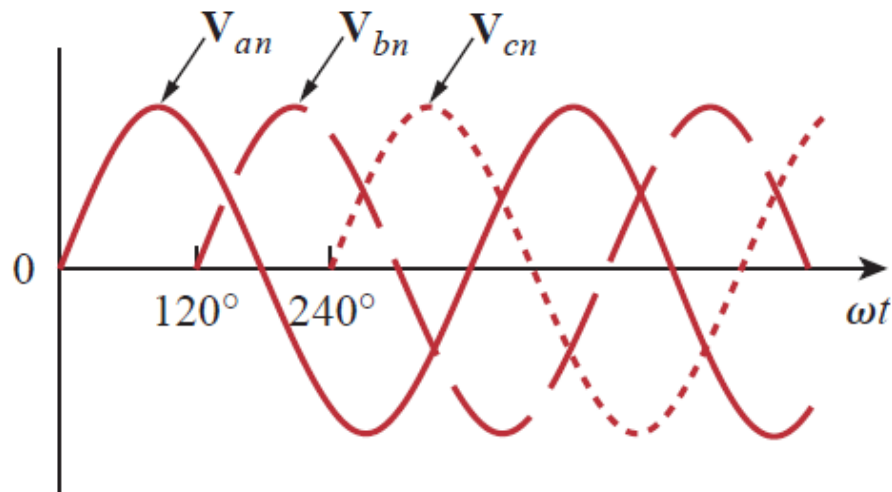
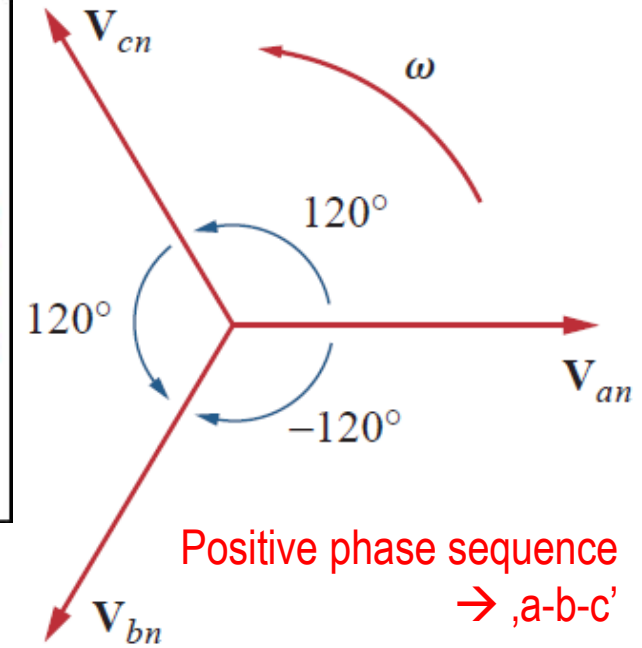
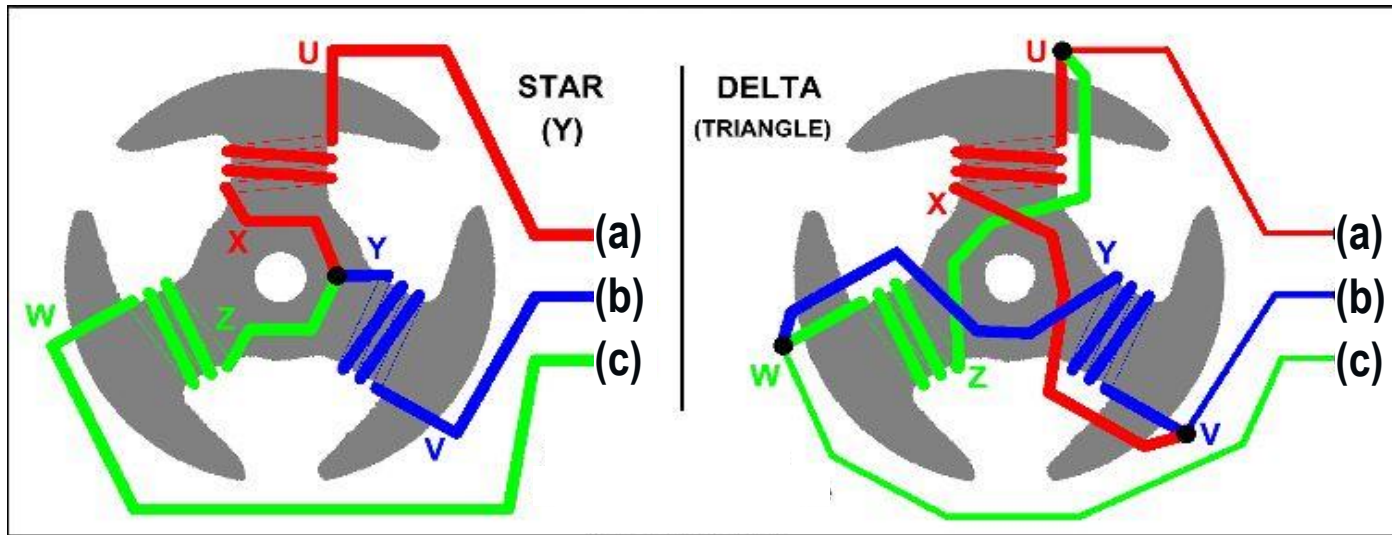




## **Balanced Three-Phase Voltages**

- Balanced Wye-Wye Connection
- Balanced Wye-Delta Connection
- Balanced Delta-Delta Connection
- Balanced Delta-Wye Connection
- Power in Balanced Systems
- Unbalanced Three-Phase Systems
- Power in Unbalanced Systems

# Three-Phase Voltages

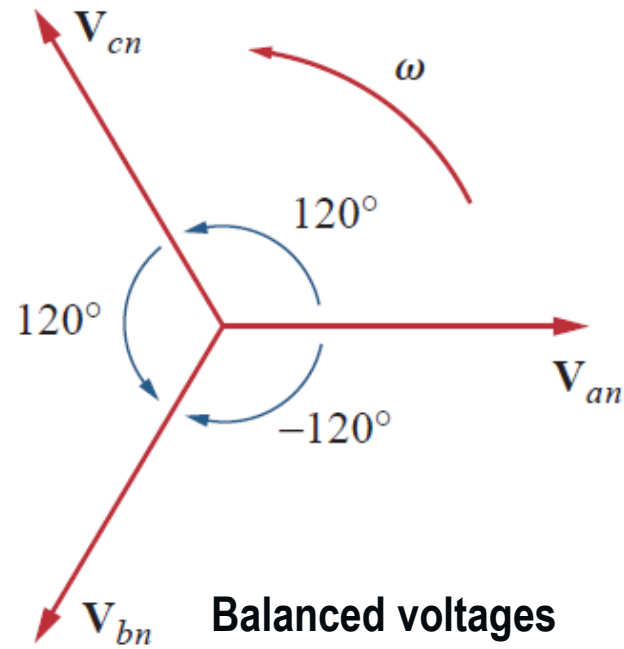
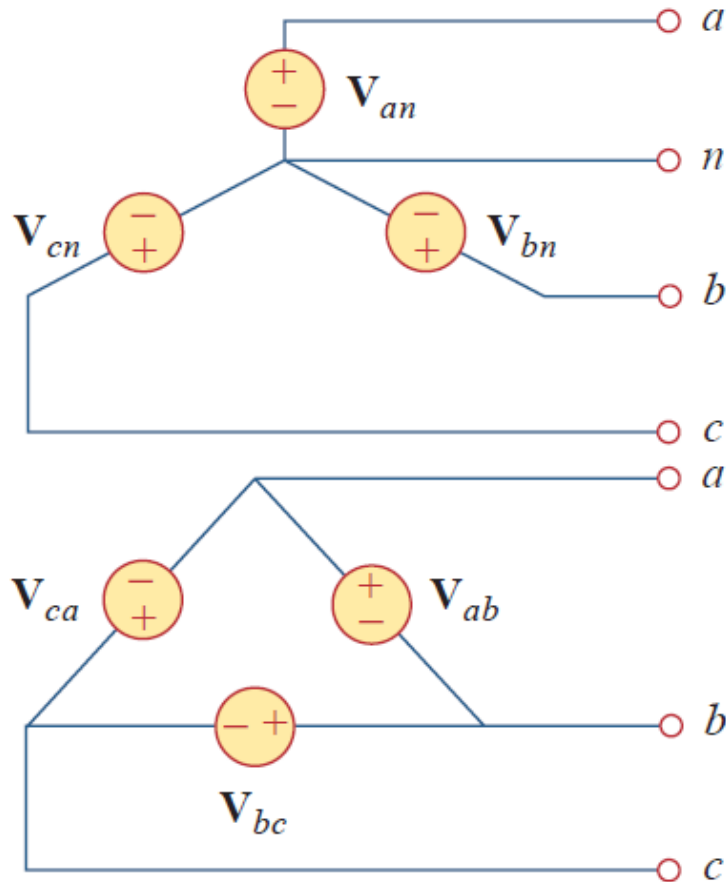


$$v_{an}(t) = V_p \sin \omega t \rightarrow \mathbf{V}_{an} = V_p e^{j0^\circ}$$

$$v_{bn}(t) = V_p \sin(\omega t - 120^\circ) \rightarrow \mathbf{V}_{bn} = V_p e^{-j120^\circ}$$

$$v_{cn}(t) = V_p \sin(\omega t + 120^\circ) \rightarrow \mathbf{V}_{cn} = V_p e^{j120^\circ}$$

# Source to Load Connections

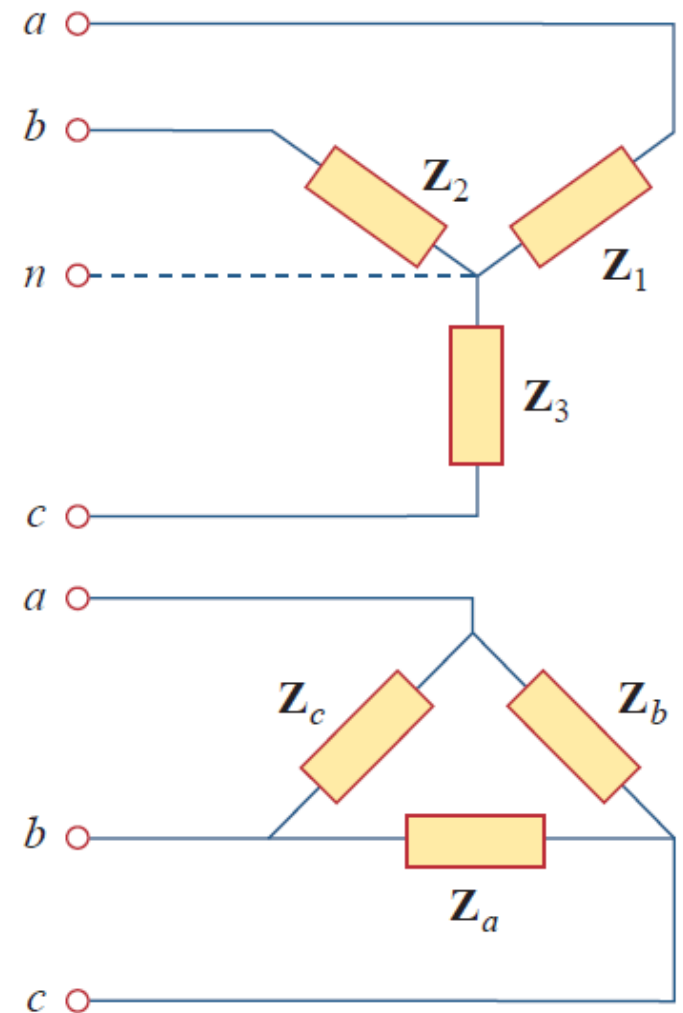


## Balanced voltages

- $V_{an} + V_{bn} + V_{cn} = 0$
- $V_{an} = V_{bn} = V_{cn} = V$

## Balanced load

- $Z_1 = Z_2 = Z_3 = Z_Y$
- $Z_a = Z_b = Z_c = Z_{\Delta}$



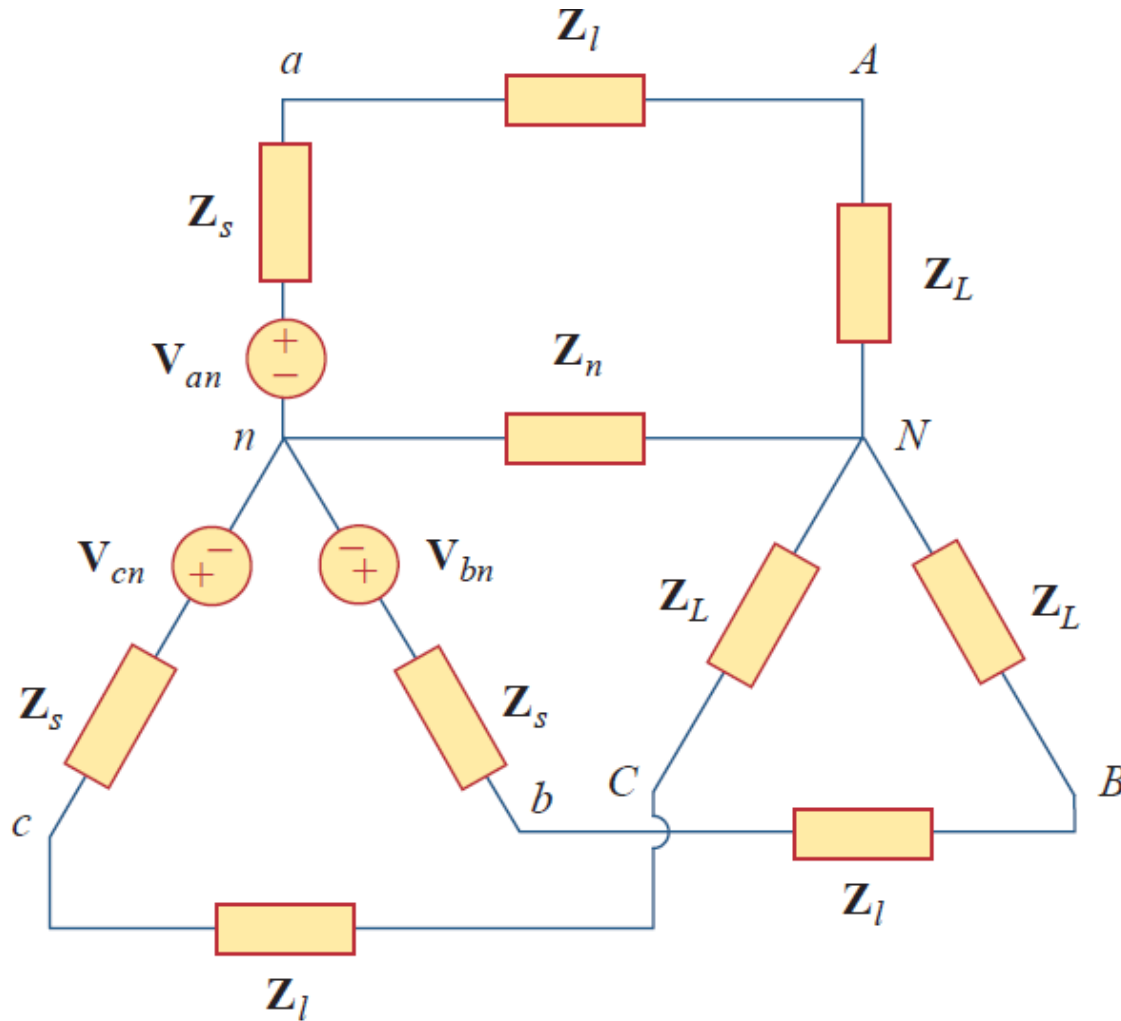
Possible source - load connections

(1) Y - Y. (2) Y - Δ, (3) Δ - Δ, (4) Δ - Y



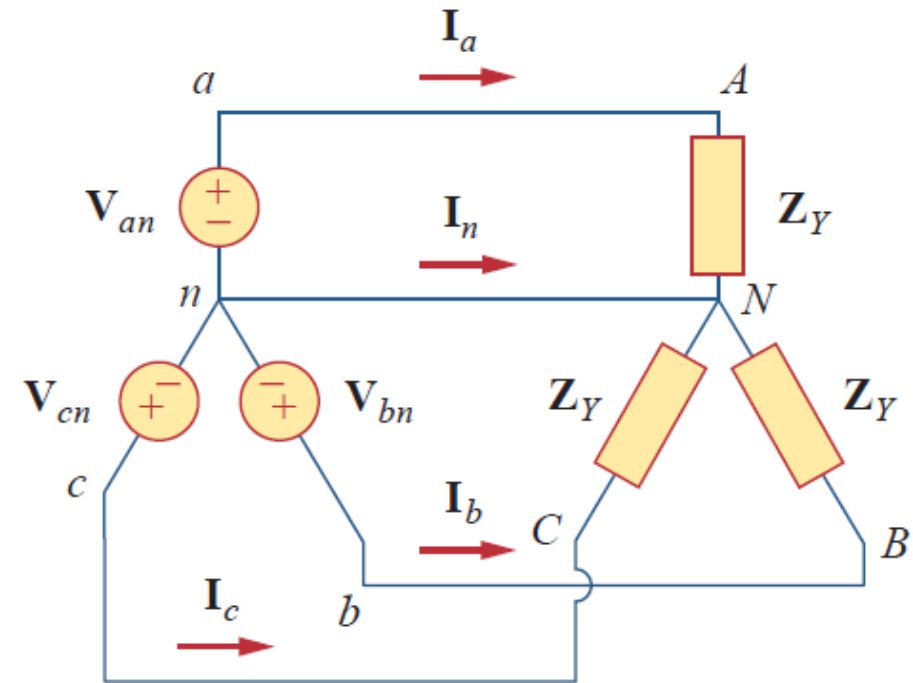
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# Balanced Wye-Wye...



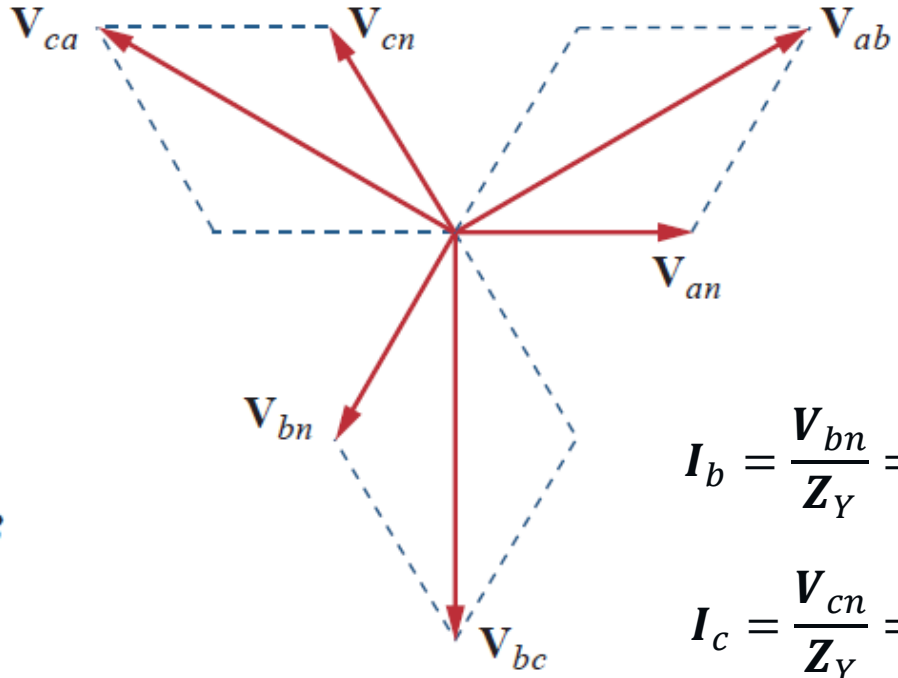
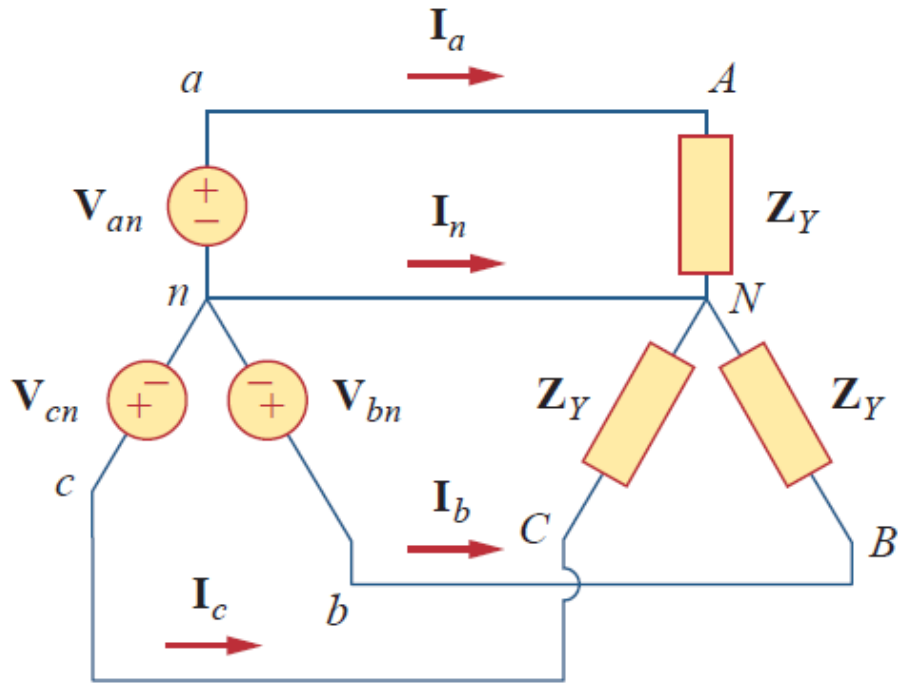
$$Z_Y = Z_S + Z_l + Z_L$$

$$Z_n \approx 0, Z_S \approx 0, Z_l \approx 0 \rightarrow Z_Y = Z_L$$





# Balanced Wye-Wye...



$$I_a = \frac{V_{an}}{Z_Y}$$

$$I_b = \frac{V_{bn}}{Z_Y} = \frac{V_{an}e^{-j120^\circ}}{Z_Y} = I_a e^{-j120^\circ}$$

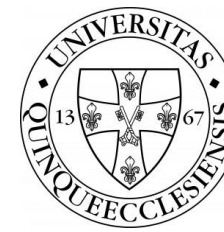
$$I_c = \frac{V_{cn}}{Z_Y} = \frac{V_{an}e^{-j240^\circ}}{Z_Y} = I_a e^{-j240^\circ}$$

$$V_{an} = V_p e^{j0^\circ}, \quad V_{bn} = V_p e^{-j120^\circ}, \quad V_{cn} = V_p e^{j120^\circ} \quad V_L = \sqrt{3}V_p, \quad I_L = I_p \quad I_a + I_b + I_c = 0$$

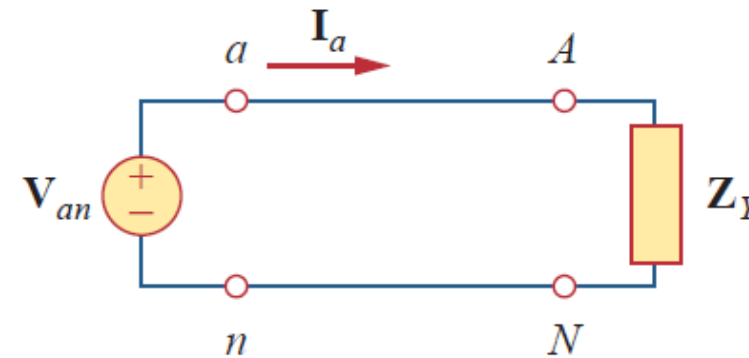
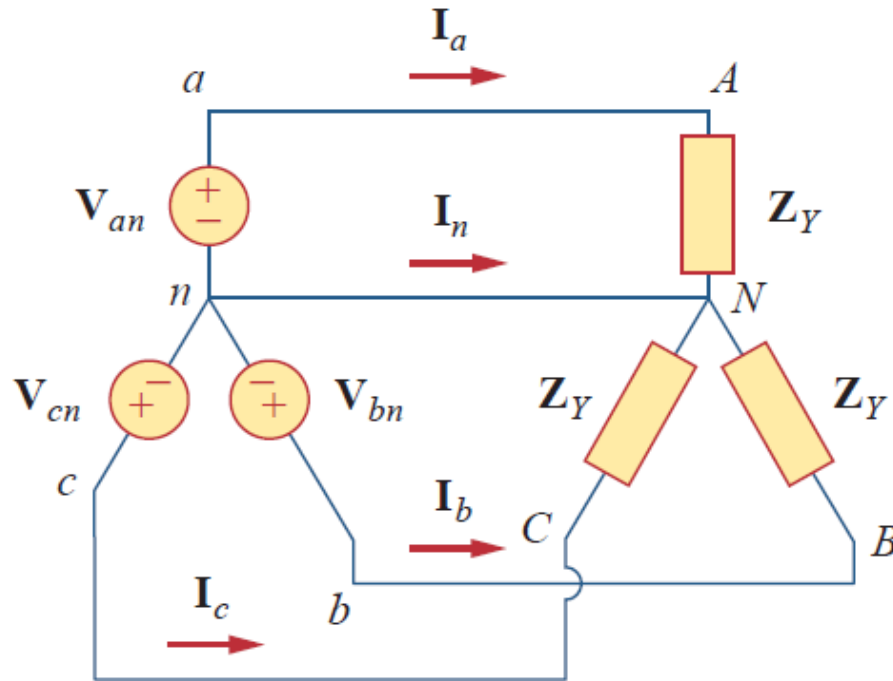
$$V_{ab} = V_{an} - V_{bn} = V_p e^{j0^\circ} - V_p e^{-j120^\circ} = V_p \left( 1 + \frac{1}{2} + j\frac{\sqrt{3}}{2} \right) = \sqrt{3}V_p e^{j30^\circ} \quad I_n = -(I_a + I_b + I_c) = 0$$

$$V_{bc} = V_{bn} - V_{cn} = \dots = \sqrt{3}V_p e^{-j90^\circ} \quad V_{ca} = V_{cn} - V_{an} = \dots = \sqrt{3}V_p e^{-j210^\circ} \quad V_{nN} = Z_n I_n = 0$$

# Balanced Wye-Wye...



Single phase equivalent



$$I_a = \frac{V_{an}}{Z_Y}$$

$$I_b = I_a e^{-j120^\circ}, \quad I_c = I_a e^{-j240^\circ}$$

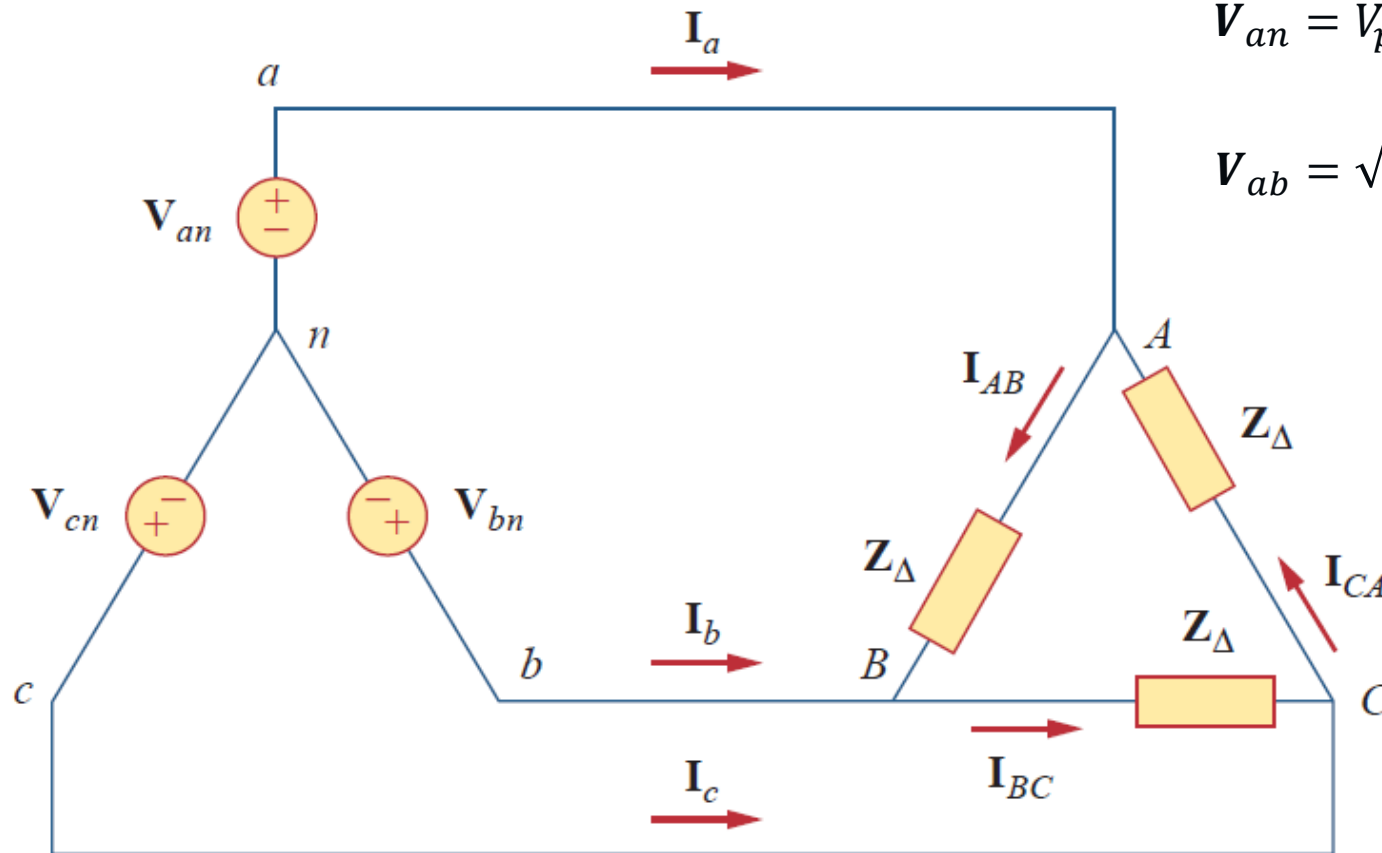


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# Balanced Wye-Delta...



The most practical and most commonly used three-phase system.



$$V_{an} = V_p e^{j0^\circ}, \quad V_{bn} = V_p e^{-j120^\circ}, \quad V_{cn} = V_p e^{j120^\circ}$$

$$V_{ab} = \sqrt{3}V_p e^{j30^\circ} = V_{AB}, \quad V_{bc} = \sqrt{3}V_p e^{-j90^\circ} = V_{BC}$$

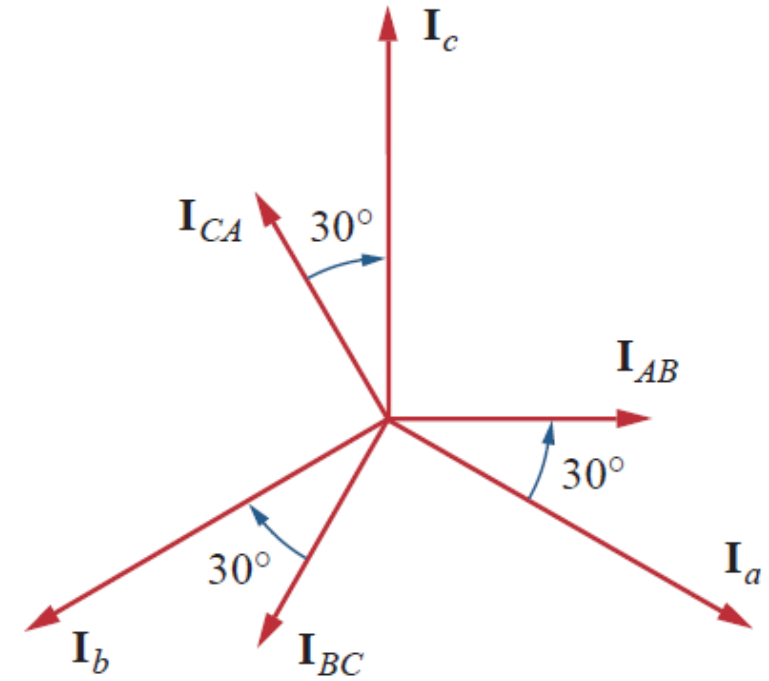
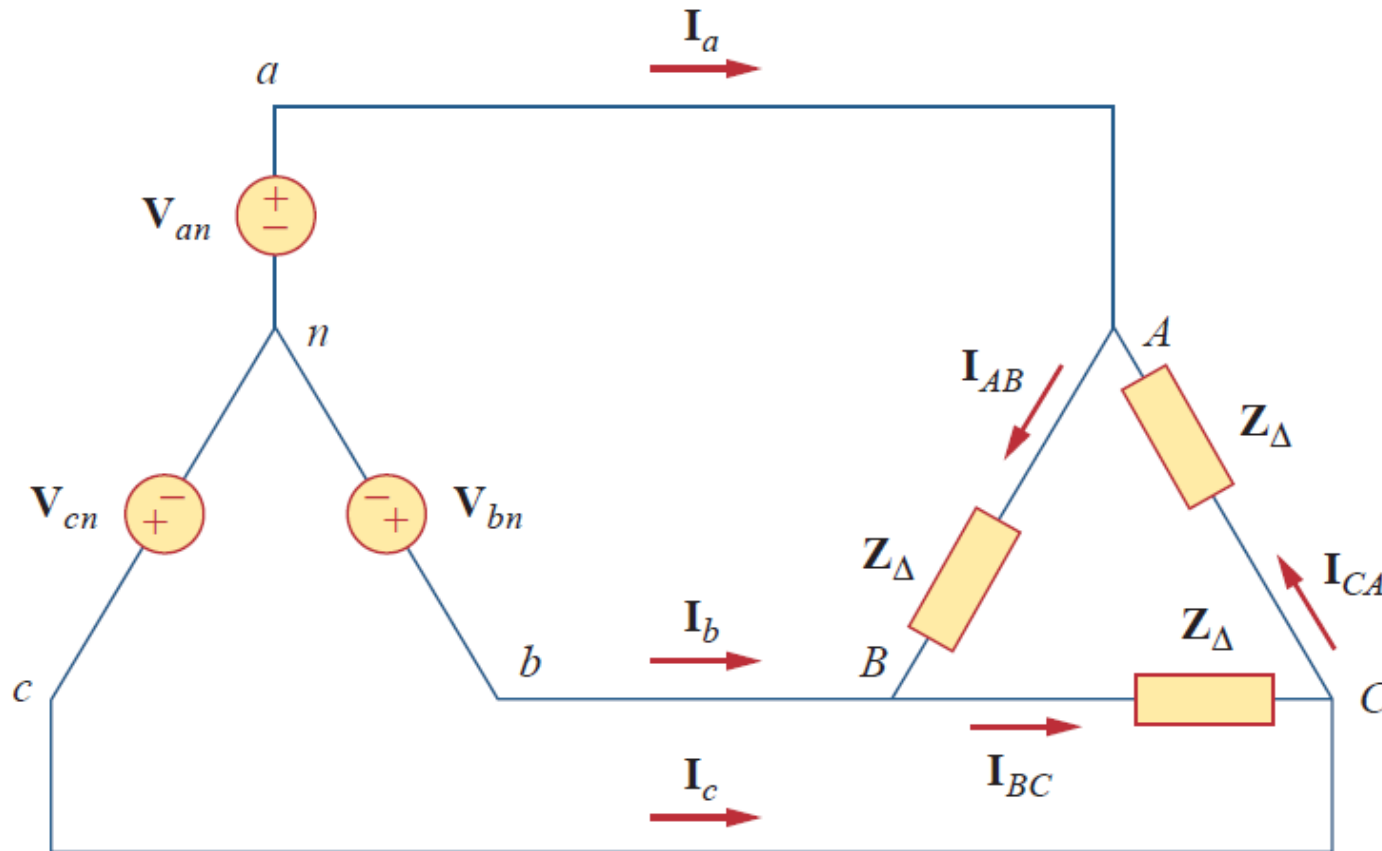
$$V_{ca} = \sqrt{3}V_p e^{j150^\circ} = V_{CA}$$

$$I_{AB} = \frac{V_{AB}}{Z_\Delta}, \quad I_{BC} = \frac{V_{BC}}{Z_\Delta}, \quad I_{CA} = \frac{V_{CA}}{Z_\Delta}$$

Another way...  $-V_{an} + Z_\Delta I_{AB} + V_{bn} = 0$

$$I_{AB} = \frac{V_{an} - V_{bn}}{Z_\Delta} = \frac{V_{ab}}{Z_\Delta} = \frac{V_{AB}}{Z_\Delta}$$

# Balanced Wye-Delta...



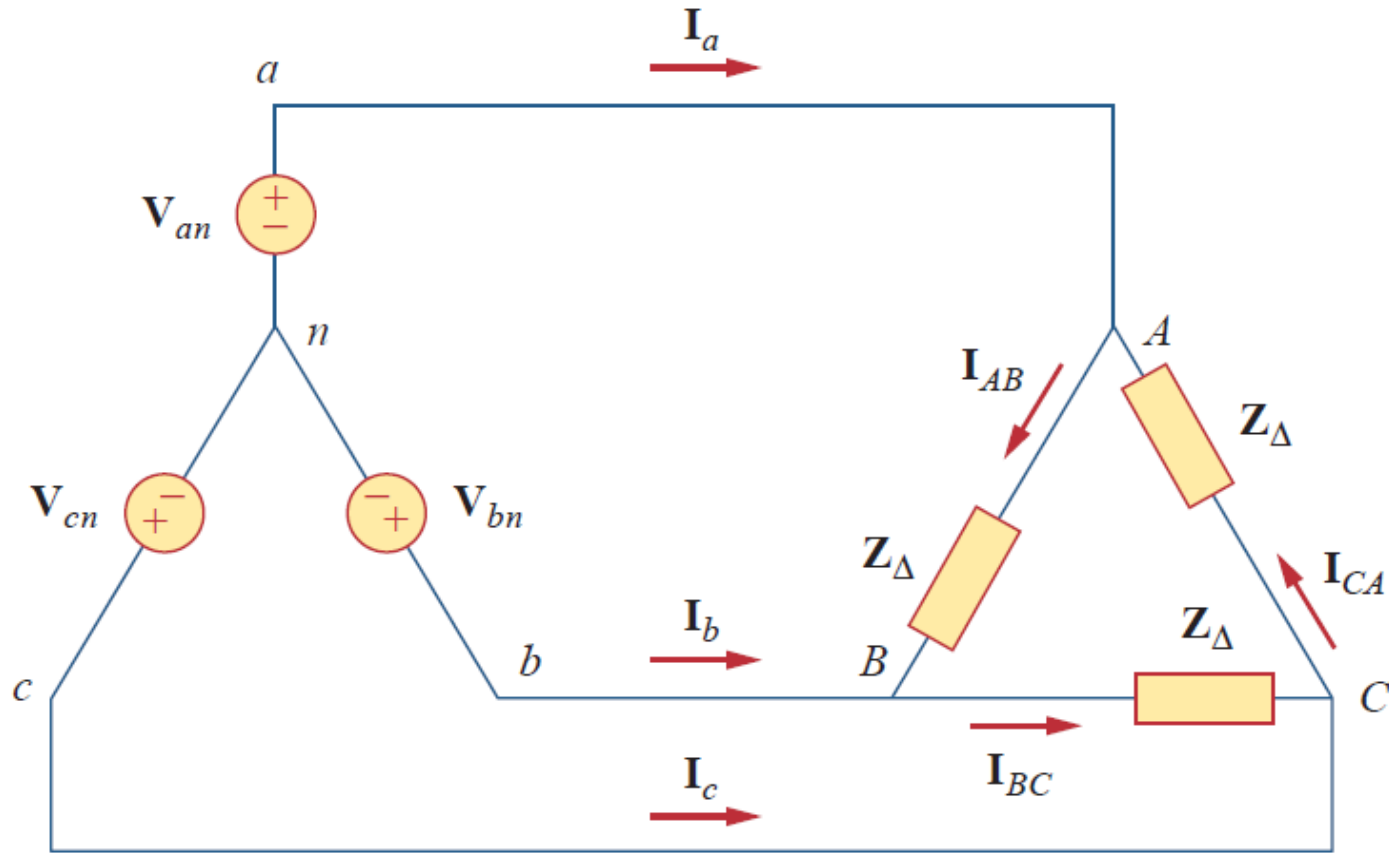
$$I_L = \sqrt{3}I_P$$

$$V_L = V_P$$

$$I_a = I_{AB} - I_{CA}, \quad I_b = I_{BC} - I_{AB}, \quad I_c = I_{CA} - I_{BC}$$

$$I_{CA} = I_{AB}e^{-j240^\circ} \rightarrow I_a = I_{AB} - I_{CA} = I_{AB}(1 - e^{-j240^\circ}) = I_{AB}(1 + 0.5 - j0.866) = I_{AB}\sqrt{3}e^{-j30^\circ}$$

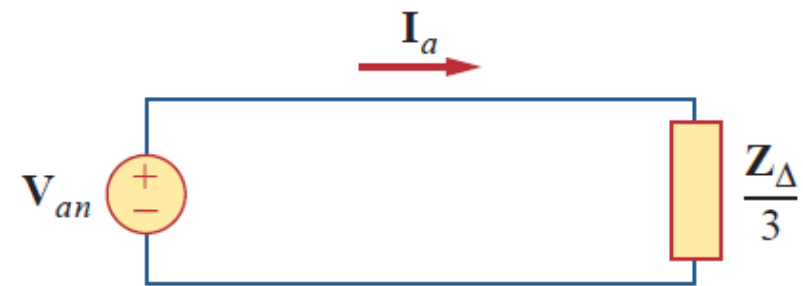
# Balanced Wye-Delta...



- Wye – delta equivalent transform

$$Z_Y = \frac{Z_\Delta}{3}$$

- Single phase equivalent

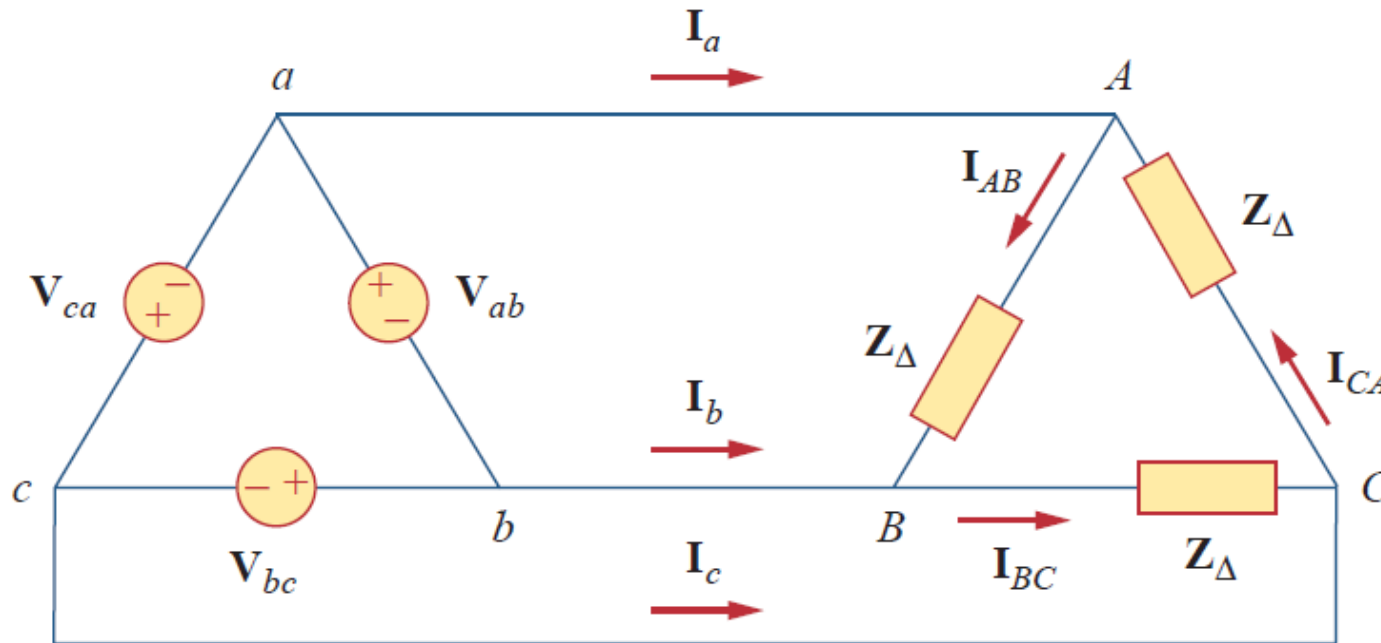
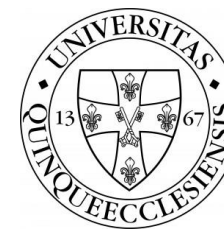


$$I_a = \frac{V_{an}}{Z_Y}$$



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# Balanced Delta-Delta...



$$I_{AB} = \frac{V_{AB}}{Z_{\Delta}} = \frac{V_{ab}}{Z_{\Delta}} \quad I_a = I_{AB} - I_{CA}$$

$$I_{BC} = \frac{V_{BC}}{Z_{\Delta}} = \frac{V_{bc}}{Z_{\Delta}} \quad I_b = I_{BC} - I_{AB}$$

$$I_{CA} = \frac{V_{CA}}{Z_{\Delta}} = \frac{V_{ca}}{Z_{\Delta}} \quad I_c = I_{CA} - I_{BC}$$

$$V_{ab} = V_p e^{j0^\circ}, \quad V_{bc} = V_p e^{-j120^\circ}, \quad V_{ca} = V_p e^{j120^\circ}$$

$$V_{ab} = V_{AB}, \quad V_{bc} = V_{BC}, \quad V_{ca} = V_{CA}$$

$$I_L = \sqrt{3} I_P$$

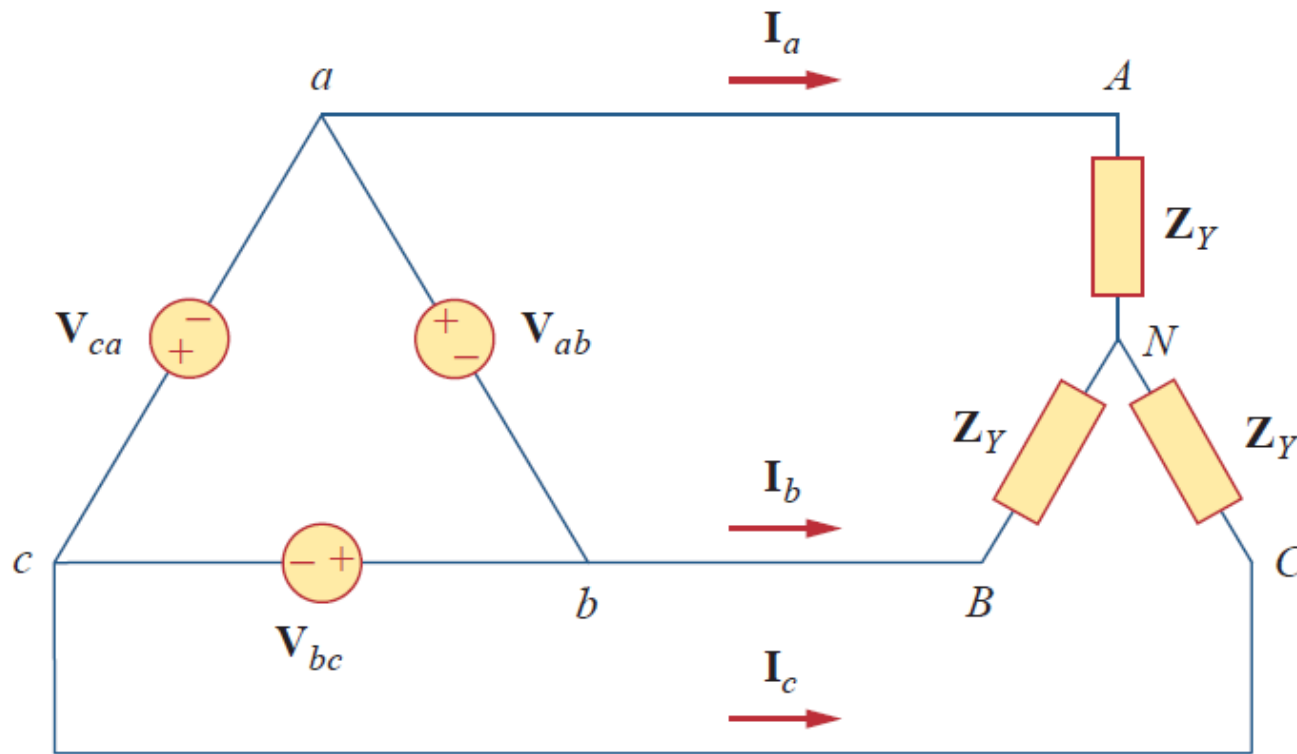
$$V_L = V_P$$





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# Balanced Delta-Wye...



$$V_{ab} = V_p e^{j0^\circ}, \quad V_{bc} = V_p e^{-j120^\circ}, \quad V_{ca} = V_p e^{j120^\circ}$$

$$-V_{ab} + Z_Y I_a - Z_Y I_b = 0 \rightarrow Z_Y (I_a - I_b) = V_{ab} = V_p e^{j0^\circ}$$

$$I_a - I_b = \frac{V_p e^{j0^\circ}}{Z_Y}$$

$$I_b = I_a e^{-j120^\circ}$$

$$\rightarrow I_a - I_b = I_a (1 + 0.5 + j0.866)$$

$$= I_a \sqrt{3} e^{j30^\circ}$$

$$I_a = \frac{V_p / \sqrt{3} e^{-j30^\circ}}{Z_Y}$$

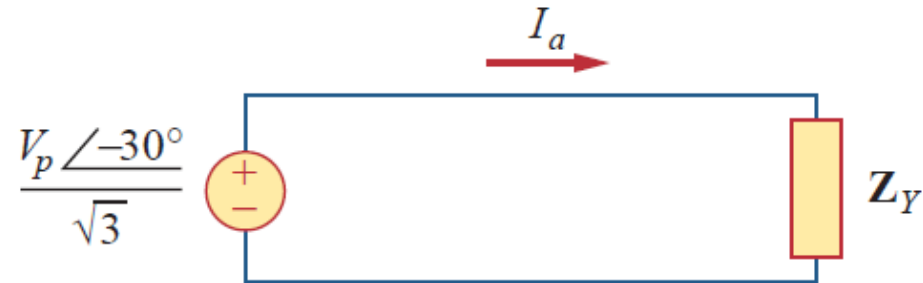
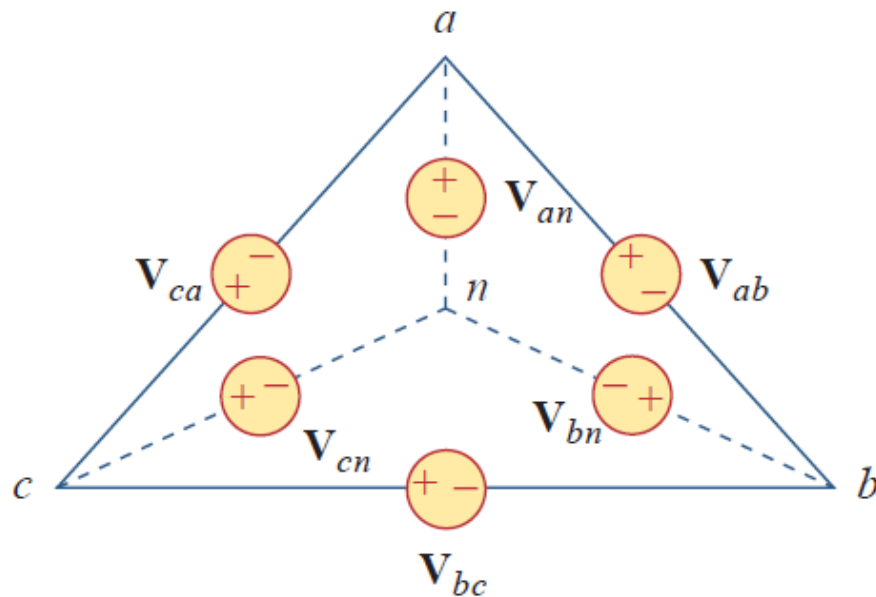
$$I_b = I_a e^{-j120^\circ}$$

$$I_c = I_a e^{j120^\circ}$$

# Balanced Delta-Wye...



Delta – Wye – source transform  $V_{an} = \frac{V_p}{\sqrt{3}} e^{-j30^\circ}$ ,  $V_{bn} = \frac{V_p}{\sqrt{3}} e^{-j150^\circ}$ ,  $V_{cn} = \frac{V_p}{\sqrt{3}} e^{j90^\circ}$



$$I_a = \frac{V_p / \sqrt{3} e^{-j30^\circ}}{Z_Y}$$

$$V_{BN} = V_{AN} e^{-j120^\circ}$$

$$V_{AN} = I_a Z_Y = \frac{V_p}{\sqrt{3}} e^{-j30^\circ}$$

$$V_{CN} = V_{AN} e^{j120^\circ}$$



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# Power in a Balanced System



Instantaneous power for Y connected load

$$v_{AN} = V_p \sqrt{2} \cos \omega t, \quad v_{BN} = V_p \sqrt{2} \cos(\omega t - 120^\circ), \quad v_{CN} = V_p \sqrt{2} \cos(\omega t + 120^\circ)$$

$$i_a = I_p \sqrt{2} \cos(\omega t - \theta), \quad i_b = I_p \sqrt{2} \cos(\omega t - \theta - 120^\circ), \quad i_c = I_p \sqrt{2} \cos(\omega t - \theta + 120^\circ)$$

$$p = p_a + p_b + p_c = v_{AN} i_a + v_{BN} i_b + v_{CN} i_c =$$

$$= 2V_p I_p [\cos \omega t \cos(\omega t - \theta) + \cos(\omega t - 120^\circ) \cos(\omega t - \theta - 120^\circ) + \cos(\omega t + 120^\circ) \cos(\omega t - \theta + 120^\circ)]$$

$$\cos A \cos B = \frac{1}{2} [\cos(A + B) + \cos(A - B)]$$

$$p = V_p I_p [3 \cos \theta + \cos(2\omega t - \theta) + \cos(2\omega t - \theta - 240^\circ) + \cos(2\omega t - \theta + 240^\circ)]$$

$$\cos(A \mp B) = \cos A \cos B \pm \sin A \sin B, \quad \cos(2\omega t - \theta) = \cos \alpha$$

$$p = V_p I_p [3 \cos \theta + \cos(\alpha) + \cos(\alpha - 240^\circ) + \cos(\alpha + 240^\circ)] = V_p I_p \left[ 3 \cos \theta + \cos(\alpha) + 2 \left( -\frac{1}{2} \right) \cos(\alpha) \right]$$

$$p = 3V_p I_p \cos \theta$$

# Power in a Balanced System



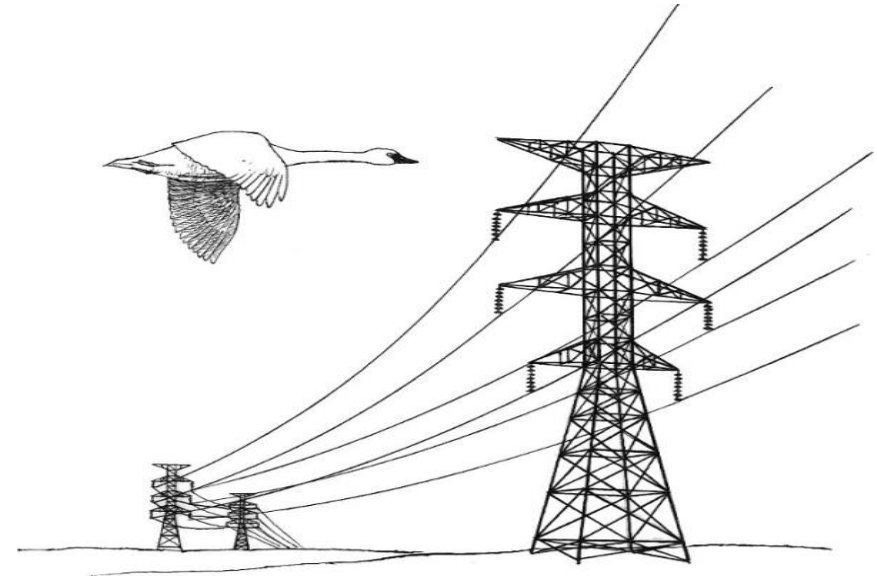
$$p = 3V_p I_p \cos \theta$$

$$\text{average PWR per phase} \rightarrow P_p = \frac{p}{3} = V_p I_p \cos \theta$$

$$\text{reactive PWR per phase} \rightarrow Q_p = V_p I_p \sin \theta$$

$$\text{apparent PWR per phase} \rightarrow S_p = V_p I_p$$

$$\text{complex PWR per phase} \rightarrow \mathbf{S}_p = P_p + jQ_p = \mathbf{V}_p \mathbf{I}_p^*$$



$$\text{total average PWR} \rightarrow P = P_a + P_b + P_c = 3P_p = 3V_p I_p \cos \theta = \sqrt{3}V_L I_L \cos \theta \leftarrow \text{next page}$$

$$\text{total reactive PWR} \rightarrow Q = Q_a + Q_b + Q_c = 3Q_p = 3V_p I_p \sin \theta = \sqrt{3}V_L I_L \sin \theta \leftarrow \text{next page}$$

$$\text{total complex PWR} \rightarrow \mathbf{S} = 3\mathbf{S}_p = 3\mathbf{V}_p \mathbf{I}_p^* = 3I_p^2 \mathbf{Z}_p = \frac{3V_p^2}{\mathbf{Z}_p^*} = P + jQ = \sqrt{3}V_L I_L e^{j\theta} \leftarrow \text{next page}$$

# Note - Wye vs. Delta Loads

## Wye connected load

$$(V_L = \sqrt{3}V_P, I_L = I_P) \rightarrow S = 3V_P I_P = 3 \frac{V_L}{\sqrt{3}} I_L = \sqrt{3}V_L I_L$$

$$P = 3V_P I_P \cos \theta = 3 \frac{V_L}{\sqrt{3}} I_L \cos \theta = \sqrt{3}V_L I_L \cos \theta$$

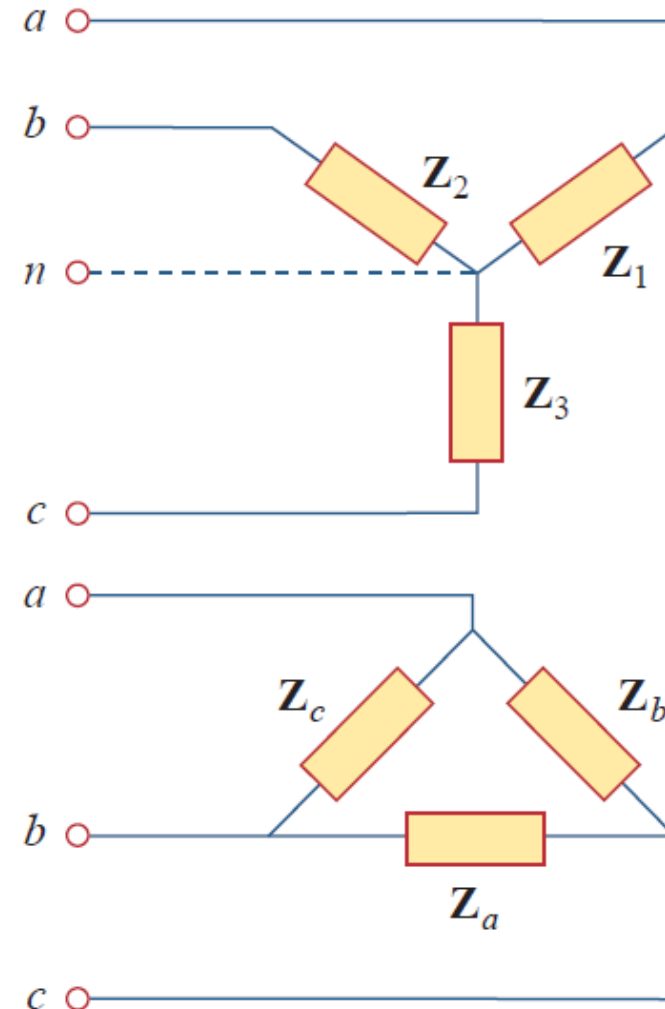
$$Q = 3V_P I_P \sin \theta = 3 \frac{V_L}{\sqrt{3}} I_L \sin \theta = \sqrt{3}V_L I_L \sin \theta$$

## Delta connected load

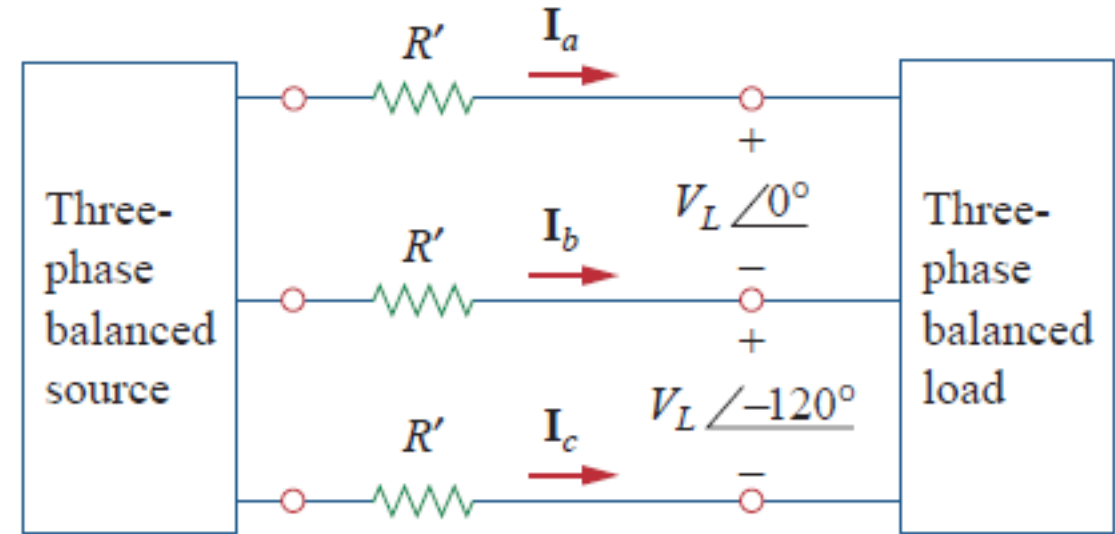
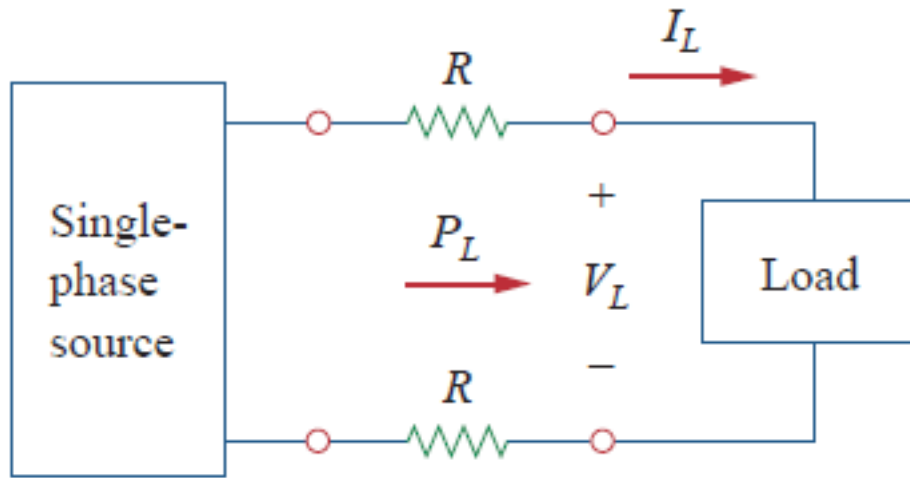
$$(V_L = V_P, I_L = \sqrt{3}I_P) \rightarrow S = 3V_P I_P = 3V_L \frac{I_L}{\sqrt{3}} = \sqrt{3}V_L I_L$$

$$P = 3V_P I_P \cos \theta = 3V_L \frac{I_L}{\sqrt{3}} \cos \theta = \sqrt{3}V_L I_L \cos \theta$$

$$Q = 3V_P I_P \sin \theta = 3V_L \frac{I_L}{\sqrt{3}} \sin \theta = \sqrt{3}V_L I_L \sin \theta$$



# Power Loss...



$$I_L = \frac{P_L}{V_L} \rightarrow P_{loss} = 2I_L^2 R = 2R \frac{P_L^2}{V_L^2}$$

$$I'_L = I_a = I_b = I_c = \frac{P_L}{\sqrt{3}V_L} \rightarrow P'_{loss} = 3(I'_L)^2 R' = 3R' \frac{P_L^2}{3V_L^2} = R' \frac{P_L^2}{V_L^2}$$

$$\frac{P_{loss}}{P'_{loss}} = \frac{2R}{R'} = \frac{2 \frac{\rho l}{\pi r^2}}{\frac{\rho l}{\pi r'^2}} = \frac{2r'^2}{r^2} \rightarrow \text{same PWR loss} \rightarrow 2r'^2 = r^2$$

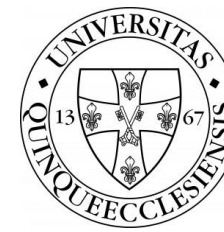
$$\frac{\text{material for single - phase}}{\text{material for three - phase}} = \frac{2(r^2 \pi l)}{3(r'^2 \pi l)} = \frac{2r^2}{3r'^2} = \frac{2}{3} \cdot 2 = 1.33 \rightarrow \text{33\% more material for single-phase transmission!}$$





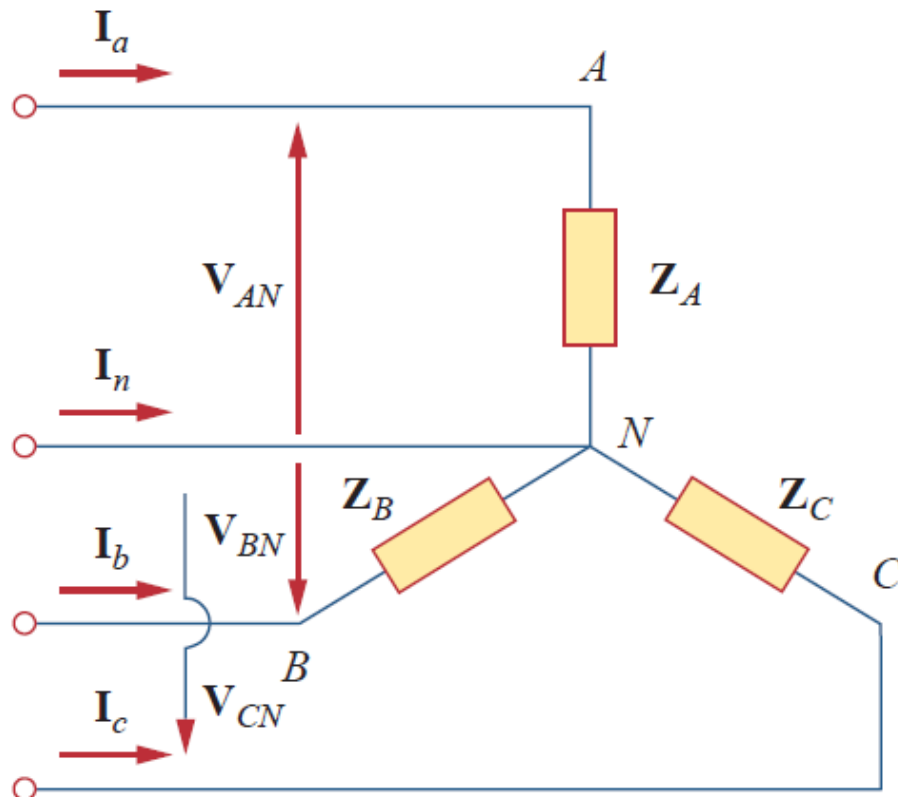
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# Unbalanced Systems



Unbalanced system is due to

- (unbalanced voltage sources)
- unbalanced load.



$$I_a = \frac{V_{AN}}{Z_A}, \quad I_b = \frac{V_{BN}}{Z_B}, \quad I_c = \frac{V_{CN}}{Z_C}$$

$$I_n = -(I_a + I_b + I_c)$$

Three-wire system  $\rightarrow I_a + I_b + I_c = 0$

*The same could be used (accordingly) for...*

- wye-connected source; wye-connected load
- delta-connected source; wye-connected load
- wye-connected source; delta-connected load
- delta-connected source; delta-connected load

# Non-Ideal Cables...



KVL + KCL + Characteristics...

$$\mathbf{Z}_A = \mathbf{Z}'_A + \mathbf{Z}_l + \mathbf{Z}_S$$

$$\mathbf{Z}_B = \mathbf{Z}'_B + \mathbf{Z}_l + \mathbf{Z}_S$$

$$\mathbf{Z}_C = \mathbf{Z}'_C + \mathbf{Z}_l + \mathbf{Z}_S$$

$$\mathbf{I}_n = \mathbf{V}_{Nn} \cdot \mathbf{Y}_n$$

$$\mathbf{I}_a = \mathbf{V}_{AN} \cdot \mathbf{Y}_A$$

$$\mathbf{I}_b = \mathbf{V}_{BN} \cdot \mathbf{Y}_B$$

$$\mathbf{I}_c = \mathbf{V}_{CN} \cdot \mathbf{Y}_C$$

$$\mathbf{V}_{an} - \mathbf{V}_{AN} + \mathbf{V}_{Nn} = 0$$

$$\mathbf{V}_{bn} - \mathbf{V}_{BN} + \mathbf{V}_{Nn} = 0$$

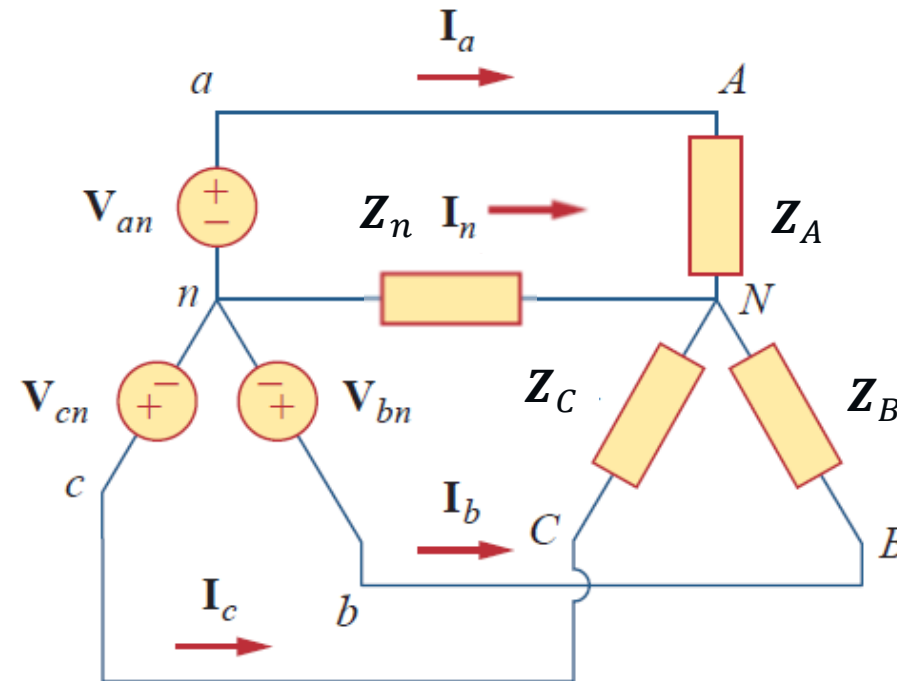
$$\mathbf{V}_{cn} - \mathbf{V}_{CN} + \mathbf{V}_{Nn} = 0$$

$$\mathbf{I}_n = -(\mathbf{I}_a + \mathbf{I}_b + \mathbf{I}_c)$$

$$\mathbf{I}_a = (\mathbf{V}_{an} + \mathbf{V}_{Nn}) \cdot \mathbf{Y}_A$$

$$\mathbf{I}_b = (\mathbf{V}_{bn} + \mathbf{V}_{Nn}) \cdot \mathbf{Y}_B$$

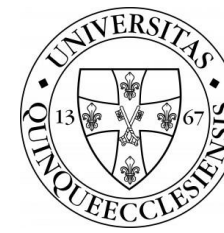
$$\mathbf{I}_c = (\mathbf{V}_{cn} + \mathbf{V}_{Nn}) \cdot \mathbf{Y}_C$$



(Millman's Theorem)

$$\mathbf{V}_{Nn} = \frac{\mathbf{V}_{an} \cdot \mathbf{Y}_A + \mathbf{V}_{bn} \cdot \mathbf{Y}_B + \mathbf{V}_{cn} \cdot \mathbf{Y}_C}{\mathbf{Y}_A + \mathbf{Y}_B + \mathbf{Y}_C + \mathbf{Y}_n}$$

# Non-Ideal Cables...



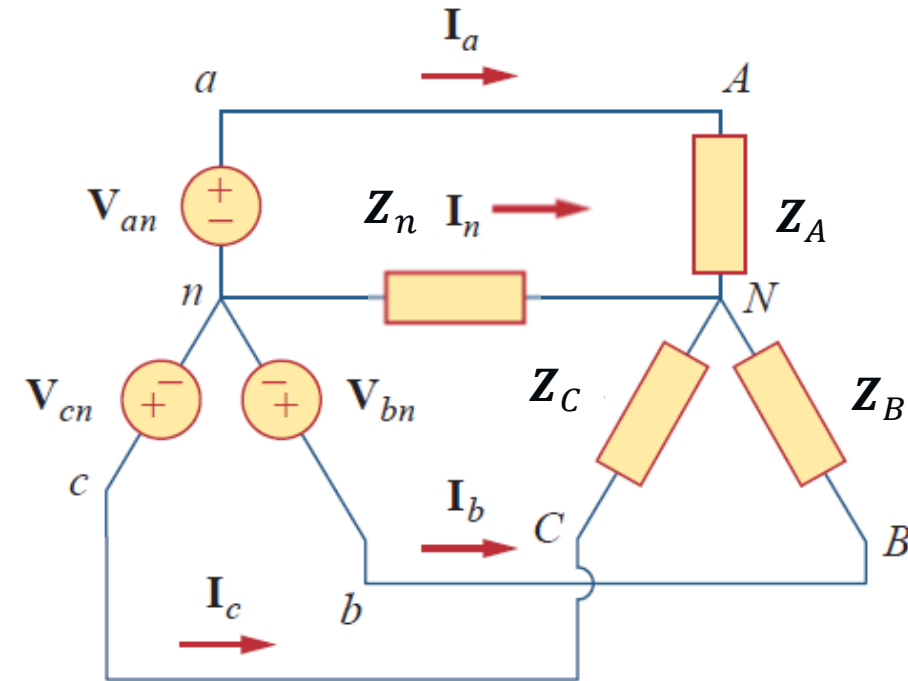
$$V_{Nn} = \frac{V_{an} \cdot Y_A + V_{bn} \cdot Y_B + V_{cn} \cdot Y_C}{Y_A + Y_B + Y_C + Y_n}$$

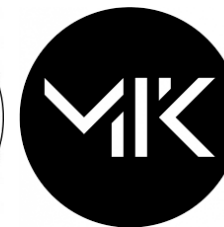
□ In case of balanced load

$$Y_A = Y_B = Y_C \rightarrow V_{Nn} = \frac{Y_A \cdot (V_{an} + V_{bn} + V_{cn})}{3 \cdot Y_A + Y_n} = 0$$

□ In case of unbalanced load + ideal neutral wire

$$Y_N = \infty \rightarrow V_{Nn} = 0, \quad I_n > 0$$



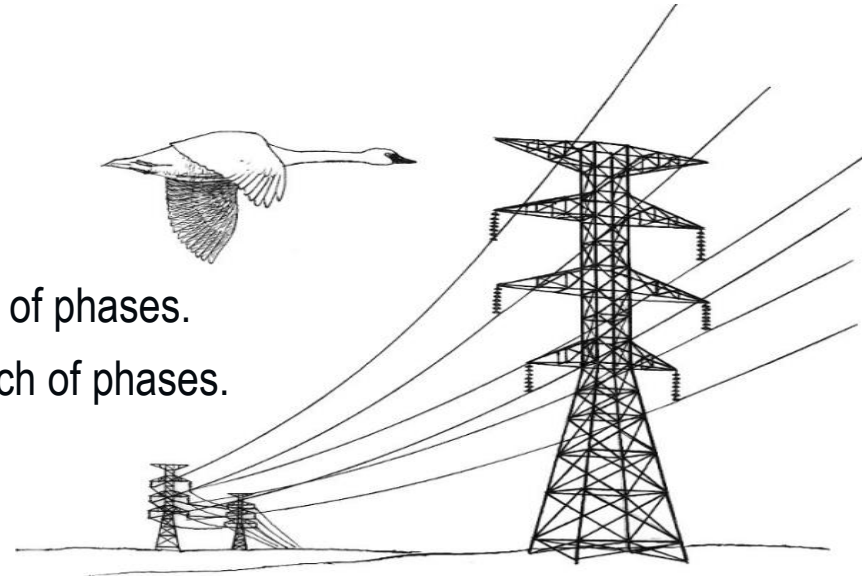


- Balanced Three-Phase Voltages
- Balanced Wye-Wye Connection
- Balanced Wye-Delta Connection
- Balanced Delta-Delta Connection
- Balanced Delta-Wye Connection
- Power in Balanced Systems
- Unbalanced Three-Phase Systems
- Power in Unbalanced Systems**

# Power in Unbalanced Systems

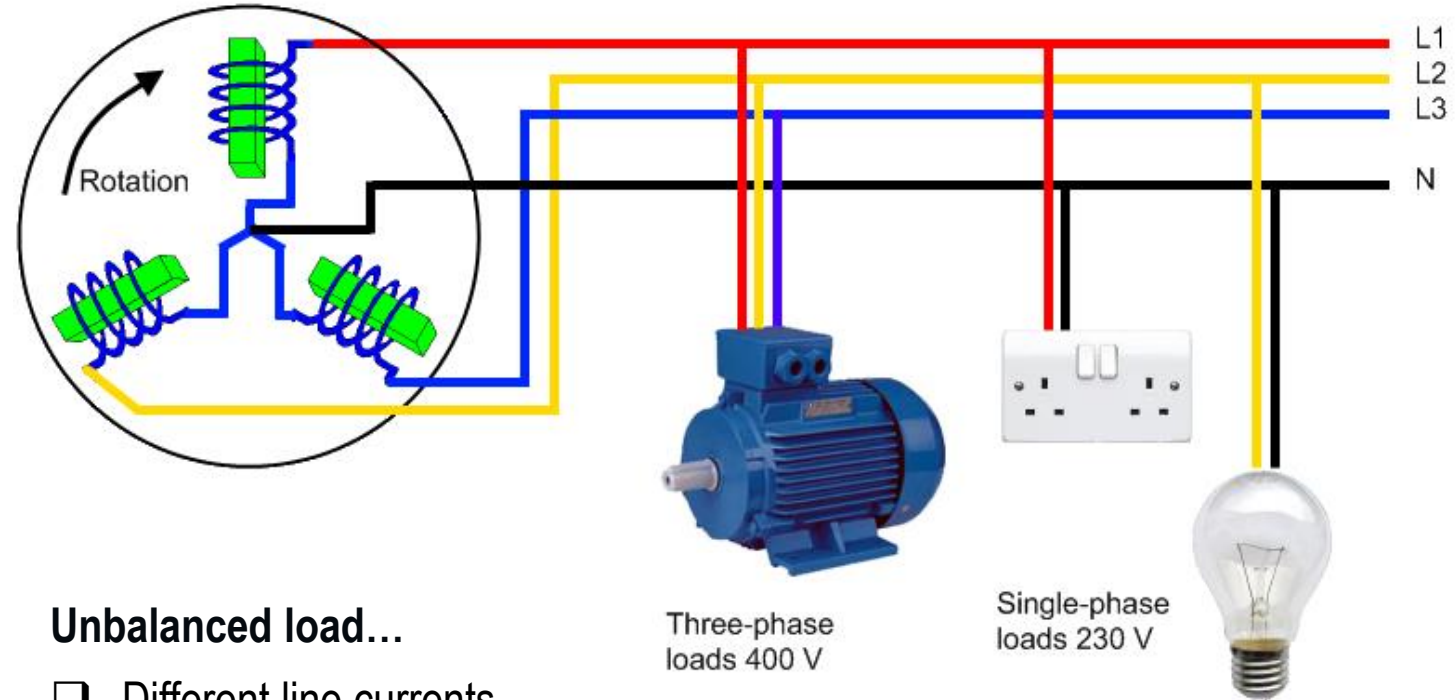
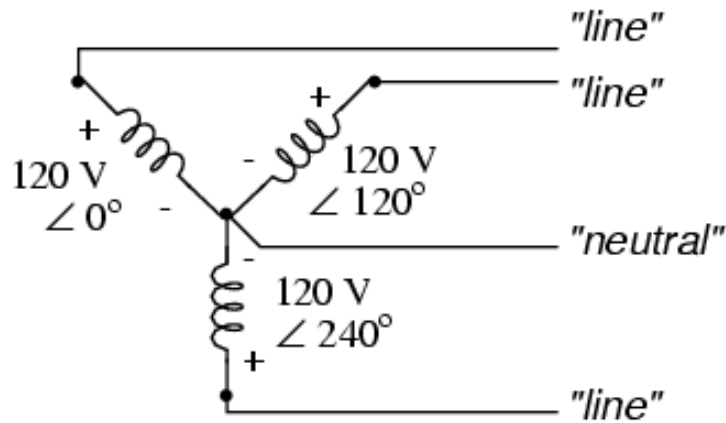


- ❑ The total PWR is not simply three times the PWR in any of phases.
- ❑ The total PWR is the sum of the unbalanced PWR in each of phases.
- ❑ Reactive PWR has sign (CAP  $\rightarrow$  (-), IND  $\rightarrow$  (+))
- ❑ (Refer to Tellegen's theorem)



- ❑ Total average PWR  $\rightarrow P = P_a + P_b + P_c$ ,  $P \neq 3P_p, P \neq 3V_p I_p \cos \theta, P \neq \sqrt{3}V_L I_L \cos \theta$
- ❑ Total reactive PWR  $\rightarrow Q = Q_a + Q_b + Q_c$ ,  $Q \neq 3Q_p, Q \neq 3V_p I_p \sin \theta, Q \neq \sqrt{3}V_L I_L \sin \theta$
- ❑ Total complex PWR  $\rightarrow \mathbf{S} = \mathbf{S}_a + \mathbf{S}_b + \mathbf{S}_c = P + jQ$ ,  $\mathbf{S} \neq 3\mathbf{S}_p, \mathbf{S} \neq 3V_p \mathbf{I}_p^*, \mathbf{S} \neq \sqrt{3}V_L I_L e^{j\theta}$

# Summary



## Balanced load...

- Voltages are  $120^\circ$  out of phase with each other
- Wye connection
  - $V_L = \sqrt{3} V_P$        $I_L = I_P$
  - Common (neutral) nodes  $\rightarrow$  same potential
  - No neutral current (3 wire/4 wire systems)
- Delta connection
  - $V_L = V_P$        $I_L = \sqrt{3} I_P$

## Unbalanced load...

- Different line currents
- Wye connection
  - Common (neutral) nodes  $\rightarrow$  different potential
  - Neutral current occurs (4 wire system)
- Total power  $\rightarrow$  sum of different powers in phases

# Questions

